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-----SOUTH AFRICA-----

GEOTECHNICAL SOIL TEST REPORT

Client: THOMAS BEMELMAN

Project: ERF 1216 SEA VISTA ST FRANCIS BAY

Date of test: 5 NOVEMBER 2023

Geotechnical Constraint	Risk			NHBC Classification
	Low	Medium	High	
Active clay	X			
Compressible soil		X		S
Collapsible soil	X			
Imported/uncontrolled fill		X		
Chemically aggressive soils		X		
Saturated soils/ groundwater seepage	X			
Shallow hard rock/ difficult excavations	X			
Slope stability problems	X			
Flood potential	X			
Seismicity	X			
Dolomitic land	X			

Site description:

The site, erf 1216 is in Santarem, St Francis Bay, close to the sea and at approximately 3-4m above mean sea level.

At the time of the investigation the erf was vacant.

The ground surface is generally flat with coastal vegetation (see Fig 1).

Access to the site was easily gained from the northern boundary of the site, on asphalt roads.

At the time of the investigation, the surface conditions of the erf were dry with no signs of any significant drainage issues, scour, or unstable ground problems.

FIGURE 1



Methods of investigation:

Two shallow test pits were excavated by hand to a max depth of NGL-1.2m.

A total of 4 no. DCP penetration test was conducted across the site (refer to attachment).

Results:

The geology of the site consisted of thick deposits of estuarine/dune sand.

The soil profile exposed in the test pits consisted almost entirely of good graded, sand with no clay.

No bedrock or groundwater was encountered in any of the test holes at a depth of 1,5 m, at the time of the investigation.

Although there might still be the good possibility of encountering small outcrops of hard rock at shallow depths.

The site is well drained with generally good soil permeability.

The groundwater table is expected at 1,5 to 3m NGL with seasonal and tidal fluctuations expected.

DCP tests indicated that the soil consistency was good and being medium dense.

with penetration rates of 10-30mm/blow starting from approximately 500 mm below NGL.

Recommendations:

Earthworks: Minor earthworks are anticipated to clear, level and prepare the site surface for construction.

Earthworks could be accomplished by hand or with light machinery and all excavations to a depth of at least 3m. were provisionally classified as per SABS1200D as "soft".

Excavations below 1.5m were expected to encounter the water table.

The insitu sandy soils were deemed suitable for backfilling and compaction under floors and foundations at the optimum moisture content.

Any organic matter, foreign matter (rubbish) or large rubble fragments should be removed from potential fill material.

Excavations were expected to be highly unstable at angles steeper than 35°, and adequate battering of slopes or lateral support systems.

may be required for excavations deeper than 1m.

Foundations and floors: Single/double storey masonry structures can be found on reinforced concrete strip, pad, or raft foundations.

Strip and pad foundations should be found at a minimum embedment depth of 0.7m in well compacted in situ sands.

Bearing pressures should be limited to 120kPa, to minimize settlement.

The structural engineer can consider additional improvements or variations to the foundation preparation method as he/she sees fit.

It was recommended that the structural engineer conduct inspections of the foundation trenches and ensure suitable conditions before contractors cast foundations.

Filling under reinforced concrete surface beds should be compacted at the optimum moisture content (10-12%) to 100% of maximum dry density.

Steel reinforcement in foundations should have adequate cover (min 40mm) to prevent corrosion due to saline soil conditions.

Roads: The in-situ roadbed material was marginal G7/G8 quality sandy soil, which was loose and prone to rutting.

Imported SSG gravel material may be required to pioneer the driveway layer works. This will include an imported G5 subbase layer of at least 150mm thick (compacted to 95%MDD) and cement interlocking pavers on 20mm bedding sand.

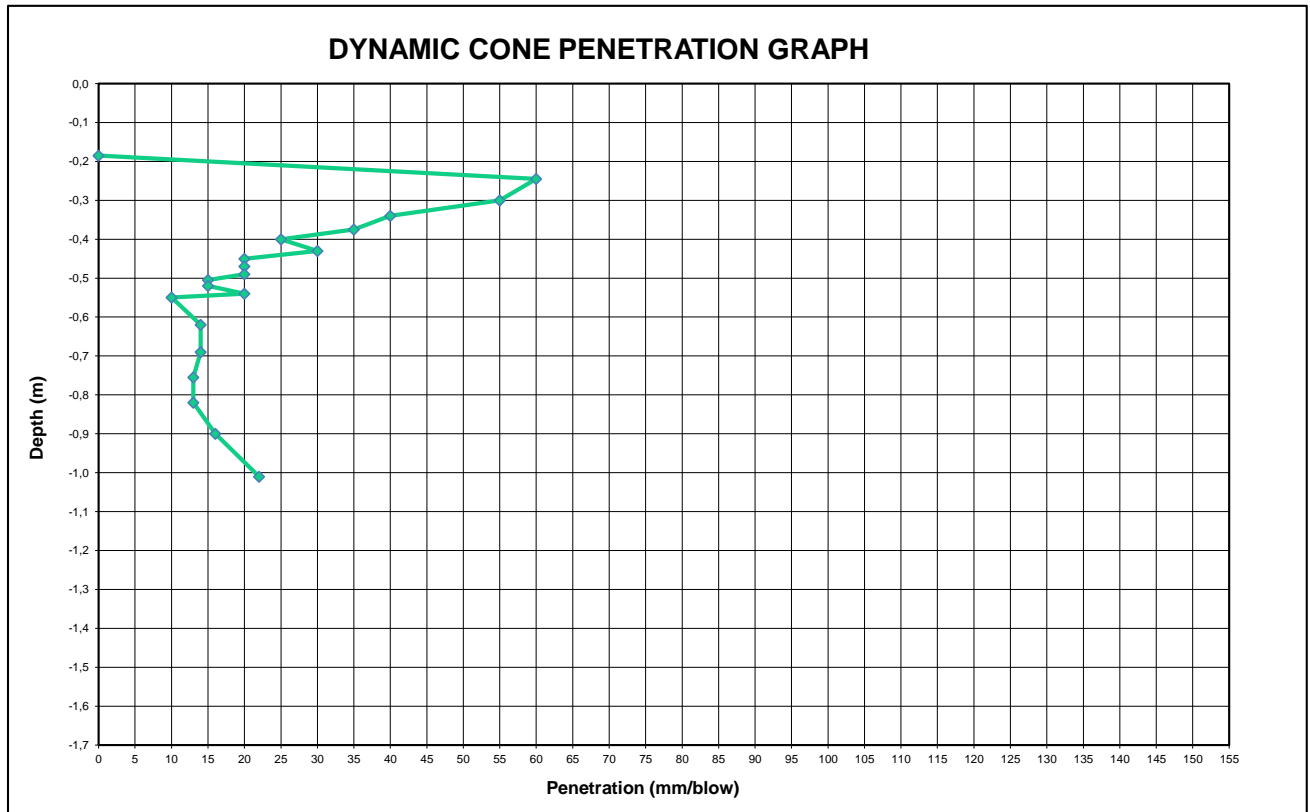
Drainage: The soil was generally highly permeable and site drainage was not envisaged to be a problem, but conventional stormwater management systems were recommended to collect and handle run-off from hard surfaces.

No subsoil drains are deemed necessary, except behind retaining walls in basement structures where necessary.

Conclusions:

The site was considered suitable for the proposed development with conventional construction methods but there were some geotechnical constraints, mainly compressible sands, which required consideration by the structural engineer and contractor.

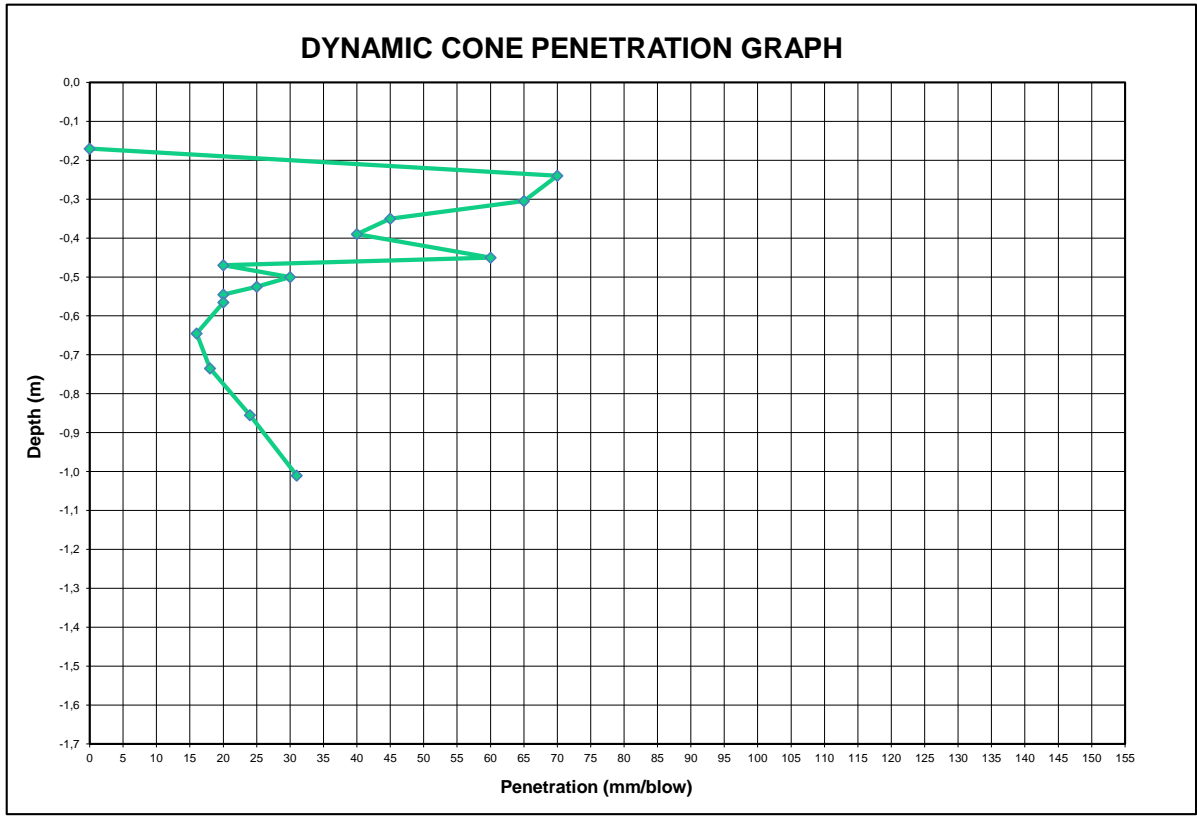
Preliminary recommendations were provided to improve founding conditions, but all information should be verified on site during construction.



TP 1 Excavation depth mm

Input Blows	Accumulated Blows	Penetration depth below test surface (mm)	Penetration depth below actual surface (mm)	Penetration rate DN (mm/blow)	Penetration depth (m)	CBR DN>2	Bearing Pressure (KPa)	Soil Consistency
0	0	185	185	0	-0,19	0,00	0,00	Test Surface
1	1	245	245	60	-0,25	2,26	30,77	Loose
1	2	300	300	55	-0,30	2,53	33,91	Loose
1	3	340	340	40	-0,34	3,79	48,40	Loose
1	4	375	375	35	-0,38	4,49	56,19	Loose
1	5	400	400	25	-0,40	6,88	81,85	Medium Dense
1	6	430	430	30	-0,43	5,46	66,76	Loose
1	7	450	450	20	-0,45	9,13	105,03	Medium Dense
1	8	470	470	20	-0,47	9,13	105,03	Medium Dense
1	9	490	490	20	-0,49	9,13	105,03	Medium Dense
1	10	505	505	15	-0,51	13,16	144,86	Medium Dense
1	11	520	520	15	-0,52	13,16	144,86	Medium Dense
1	12	540	540	20	-0,54	9,13	105,03	Medium Dense
1	13	550	550	10	-0,55	22,02	227,90	Dense
5	18	620	620	14	-0,62	14,36	156,47	Medium Dense
5	23	690	690	14	-0,69	14,36	156,47	Medium Dense
5	28	755	755	13	-0,76	15,78	169,98	Medium Dense
5	33	820	820	13	-0,82	15,78	169,98	Medium Dense
5	38	900	900	16	-0,90	12,12	134,78	Medium Dense
5	43	1010	1010	22	-1,01	8,09	94,42	Medium Dense

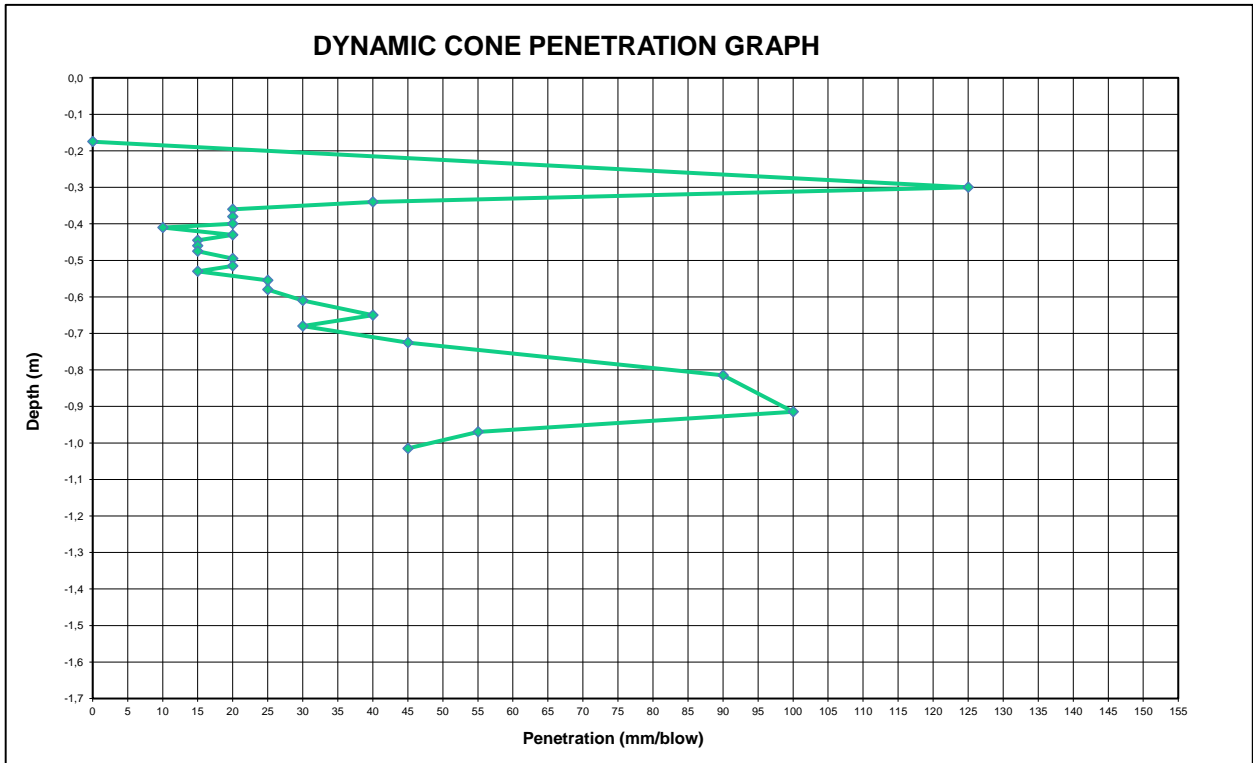
Foundation design on sand
 For single storey DN should not exceed 20 mm/blow
 For double storey DN should not exceed 15 mm/blow



TP 2 Excavation depth mm

Input Blows	Accumulated Blows	Penetration depth below test surface (mm)	Penetration depth below actual surface (mm)	Penetration rate DN (mm/blow)	Penetration depth (m)	CBR DN>2	Bearing Pressure (KPa)	Soil Consistency
0	0	170	170	0	-0,17	0,00	0,00	Test Surface
1	1	240	240	70	-0,24	1,86	25,90	Loose
1	2	305	305	65	-0,31	2,04	28,13	Loose
1	3	350	350	45	-0,35	3,26	42,43	Loose
1	4	390	390	40	-0,39	3,79	48,40	Loose
1	5	450	450	60	-0,45	2,26	30,77	Loose
1	6	470	470	20	-0,47	9,13	105,03	Medium Dense
1	7	500	500	30	-0,50	5,46	66,76	Loose
1	8	525	525	25	-0,53	6,88	81,85	Medium Dense
1	9	545	545	20	-0,55	9,13	105,03	Medium Dense
1	10	565	565	20	-0,57	9,13	105,03	Medium Dense
5	15	645	645	16	-0,65	12,12	134,78	Medium Dense
5	20	735	735	18	-0,74	10,44	118,15	Medium Dense
5	25	855	855	24	-0,86	7,24	85,67	Medium Dense
5	30	1010	1010	31	-1,01	5,23	64,36	Loose

Foundation design on sand
 For single storey DN should not exceed 20 mm/blow
 For double storey DN should not exceed 15 mm/blow



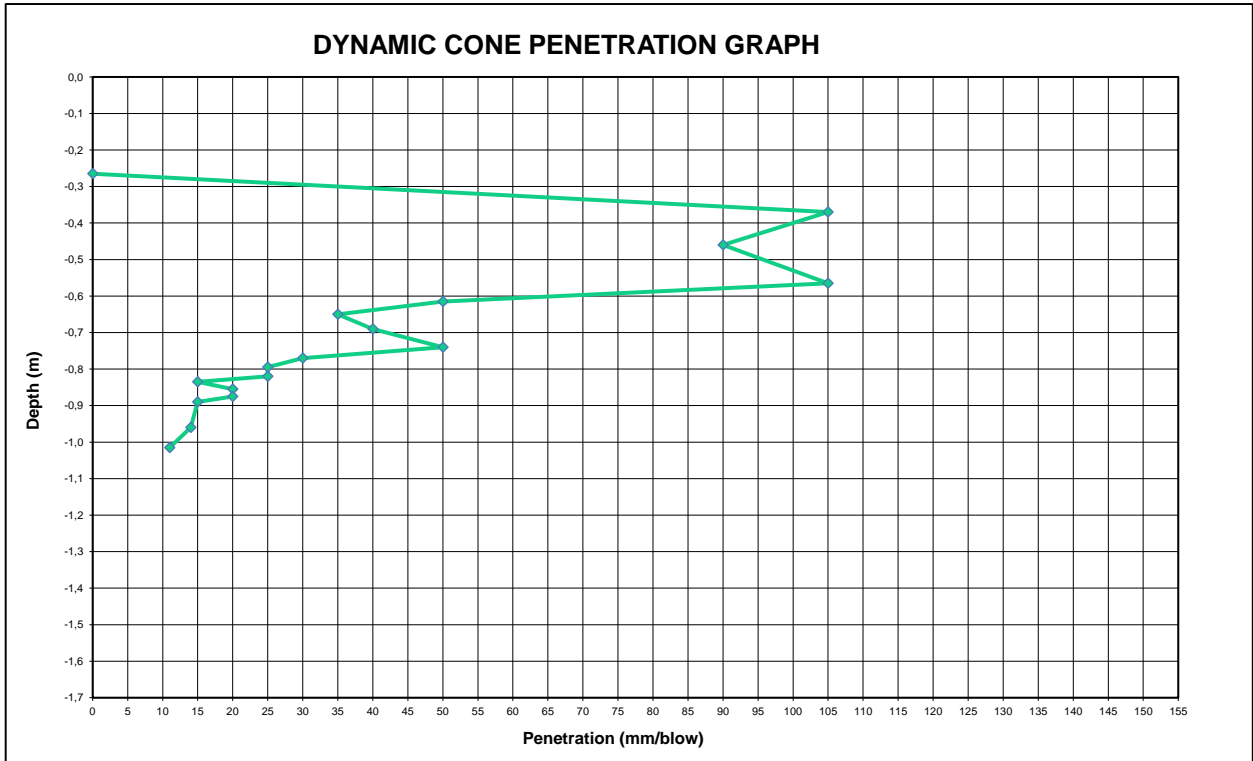
TP 3 Excavation depth mm

Input Blows	Accumulated Blows	Penetration depth below test surface (mm)	Penetration depth below actual surface (mm)	Penetration rate DN (mm/blow)	Penetration depth (m)	CBR DN>2	Bearing Pressure (KPa)	Soil Consistency
0	0	175	175	0	-0,18	0,00	0,00	Test Surface
1	1	300	300	125	-0,30	0,89	13,55	Very Loose
1	2	340	340	40	-0,34	3,79	48,40	Loose
1	3	360	360	20	-0,36	9,13	105,03	Medium Dense
1	4	380	380	20	-0,38	9,13	105,03	Medium Dense
1	5	400	400	20	-0,40	9,13	105,03	Medium Dense
1	6	410	410	10	-0,41	22,02	227,90	Dense
1	7	430	430	20	-0,43	9,13	105,03	Medium Dense
1	8	445	445	15	-0,45	13,16	144,86	Medium Dense
1	9	460	460	15	-0,46	13,16	144,86	Medium Dense
1	10	475	475	15	-0,48	13,16	144,86	Medium Dense
1	11	495	495	20	-0,50	9,13	105,03	Medium Dense
1	12	515	515	20	-0,52	9,13	105,03	Medium Dense
1	13	530	530	15	-0,53	13,16	144,86	Medium Dense
1	14	555	555	25	-0,56	6,88	81,85	Medium Dense
1	15	580	580	25	-0,58	6,88	81,85	Medium Dense
1	16	610	610	30	-0,61	5,46	66,76	Loose
1	17	650	650	40	-0,65	3,79	48,40	Loose
1	18	680	680	30	-0,68	5,46	66,76	Loose
1	19	725	725	45	-0,73	3,26	42,43	Loose
1	20	815	815	90	-0,82	1,35	19,56	Very Loose
1	21	915	915	100	-0,92	1,18	17,38	Very Loose
1	22	970	970	55	-0,97	2,53	33,91	Loose
1	23	1015	1015	45	-1,02	3,26	42,43	Loose

Foundation design on sand

For single storey DN should not exceed 20 mm/blow

For double storey DN should not exceed 15 mm/blow



TP 4

Excavation depth mm

Input Blows	Accumulated Blows	Penetration depth below test surface (mm)	Penetration depth below actual surface (mm)	Penetration rate DN (mm/blow)	Penetration depth (m)	CBR DN>2	Bearing Pressure (KPa)	Soil Consistency
0	0	265	265	0	-0,27	0,00	0,00	Test Surface
1	1	370	370	105	-0,37	1,11	16,46	Very Loose
1	2	460	460	90	-0,46	1,35	19,56	Very Loose
1	3	565	565	105	-0,57	1,11	16,46	Very Loose
1	4	615	615	50	-0,62	2,85	37,72	Loose
1	5	650	650	35	-0,65	4,49	56,19	Loose
1	6	690	690	40	-0,69	3,79	48,40	Loose
1	7	740	740	50	-0,74	2,85	37,72	Loose
1	8	770	770	30	-0,77	5,46	66,76	Loose
1	9	795	795	25	-0,80	6,88	81,85	Medium Dense
1	10	820	820	25	-0,82	6,88	81,85	Medium Dense
1	11	835	835	15	-0,84	13,16	144,86	Medium Dense
1	12	855	855	20	-0,86	9,13	105,03	Medium Dense
1	13	875	875	20	-0,88	9,13	105,03	Medium Dense
1	14	890	890	15	-0,89	13,16	144,86	Medium Dense
5	19	960	960	14	-0,96	14,36	156,47	Medium Dense
5	24	1015	1015	11	-1,02	19,51	204,87	Dense

Foundation design on sand

For single storey DN should not exceed 20 mm/blow

For double storey DN should not exceed 15 mm/blow