

GEOTECHNICAL REPORT

PROPOSED NEW RESIDENTIAL DEVELOPMENT ON PORTION 91 OF MATJIESFONTIEN 304, KEURBOOMSTRAND, PLETTENBERG BAY

8 March 2023 (Rev 0)





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Report review history:

Revision No	Date	Prepared by:	Reviewed by:	Approved by:
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Authors qualifications and affiliations:

Iain Paton has postgraduate degrees in Geology and Geotechnical Engineering and has over 25 years' experience in the mining, energy and construction industries. Iain Paton is a registered professional with the Engineering Council of South Africa (ECSA) and the South African Council for Natural and Scientific Professions (SACNSP). Iain Paton is a member of the South African Institute of Engineering and Environmental Geologists (SAIEG), the Geotechnical Division of the South African Institute of Civil Engineering (SAICE) and the Institute of Municipal Engineering of South Africa (IMESA).

Declaration of independence:

The author of this report is independent professional consultant with no vested interest in the project, other than remuneration for work associated with the compilation of this report.

General limitations:

1. The investigation has been conducted in accordance with generally accepted engineering practice, and the opinions and conclusions expressed in the report are made in good faith based on the information at hand at the time of the investigation.
2. The contents of this report are valid as of the date of preparation. However, changes in the condition of the site can occur over time as a result of either natural processes or human activity. In addition, advancements in the practice of geotechnical engineering and changes in applicable practice codes may affect the validity of this report. Consequently, this report should not be relied upon after an eclipsed period of one year without a review by this firm for verification of validity. This warranty is in lieu of all other warranties, either expressed or implied.
3. Unless otherwise stated, the investigation did not include any specialist studies, including but not limited to the evaluation or assessment of any potential environmental hazards or groundwater contamination that may be present.
4. The investigation is conducted within the constraints of the budget and time and therefore limited information was available. Although the confidence in the information is reasonably high, some variation in the geotechnical conditions should be expected during and after construction. The nature and extent of variations across the site may not become evident until construction. If variations then become apparent this could affect the proposed project, and it may be necessary to re-evaluate recommendations in this report. Therefore, it is recommended that Outeniqua Geotechnical Services is retained to provide specialist geotechnical engineering services during construction in order to observe compliance with the design concepts, specifications and recommendations and to allow design changes in the event that subsurface conditions differ from those anticipated prior to the start of construction. Any significant deviation from the expected geotechnical conditions should be brought to the author's attention for further investigation.
5. The assessment and interpretation of the geotechnical information and the design of structures and services and the management of risk is the responsibility of the appointed engineer.

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1. Introduction

1.1 Background information

A new residential development has been proposed on Portion 91 Of Matjiesfontien 304, Keurboomstrand, Plettenberg Bay. Refer to locality map in **Figure 1**. Outeniqua Geotechnical Services was appointed by the developer to conduct a broad-scope geotechnical investigation of the site. The proposed development consisted of new dwellings, internal access roads and bulk services. The physical and geotechnical nature of the site was investigated in order to facilitate the civil engineering design and project planning.

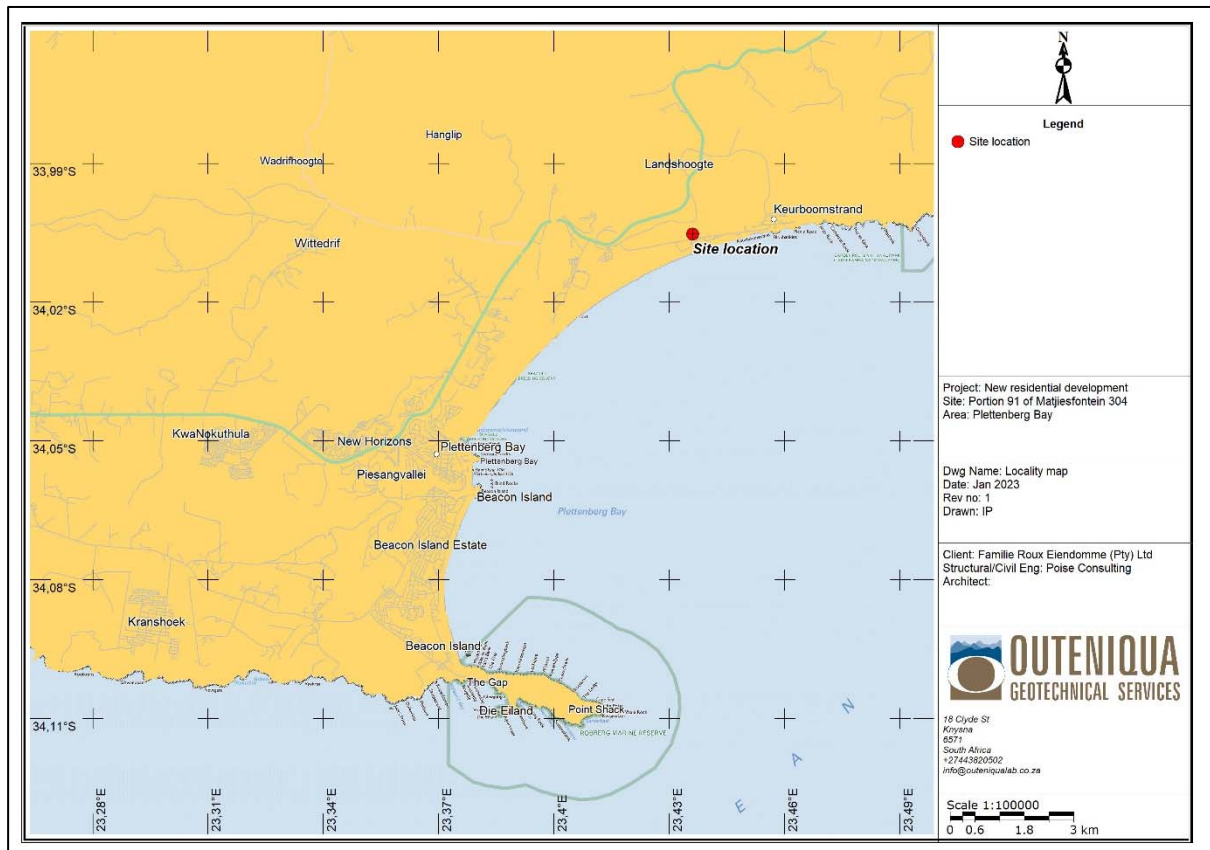


Figure 1: Locality map

1.2 Scope of work

The scope of work was to conduct a broad-scope geotechnical investigation in accordance with the SAICE Code of Practice for Site Investigations, including the following:

Desk Study:

- A desk-top review of all available information of the location, topography and geology of the site.

Site Work:

- A site reconnaissance survey to assess the general terrain and any obvious geotechnical risks associated with development of the site;
- A subsurface investigation including the excavation and profiling of a limited

- number of test pits across the site with a TLB/Backactor to a depth of 2-3m or shallower refusal, to obtain an indication of the expected geotechnical conditions;
- The collection and packaging of soil samples for laboratory testing, including:
 - Foundation Indicator tests determine gradings, Atterberg limits and potential expansiveness.
 - Modified AASHTO density, CBR & Indicator tests to determine the compaction/strength properties.
- Insitu testing, including dynamic cone penetrometer (DCP).

Professional assessment & reporting:

The assessment of data by a geotechnical engineering professional, and the preparation of a concise factual and interpretive report recommendations for:

- Foundation design for structures (including founding depths, estimated allowable safe bearing pressures).
- Any other precautions to be taken with regards to the geotechnical conditions for the proposed development.

1.3 Available information

The following maps & plans were available for consultation:

- A site locality map, provided by the developer.
- 1: 250 000 Geological Series maps of the area, obtained from the Council for Geoscience;
- Topo-cadastral data for the area, obtained from the National Geospatial Institute (NGI).
- Aerial photos of the area, obtained from the NGI and Google Earth.

2. Site description

The proposed site was located on semi-rural land in close proximity to the up-market residential area of Keurboomstrand. At the time of the investigation the site was easily accessible from the existing municipal road along the southern boundary of the site. See **Figure 2**. The site was largely vacant but was being used as a horse-riding facility with several temporary stable structures. The topography was broadly characterised by very gently sloping ground on the southern portion of the site (the proposed development portion) with an average gradient of ~1:50, and a steep northern portion (not intended for development). The ground surface on the development portion was covered in patchy short grass and a few scattered bushes and trees. The northern slopes were densely vegetated with indigenous bush (see **Figure 3 & 4**). The climate of the area was typically wet with a Weinert Climatic N-value of 2.

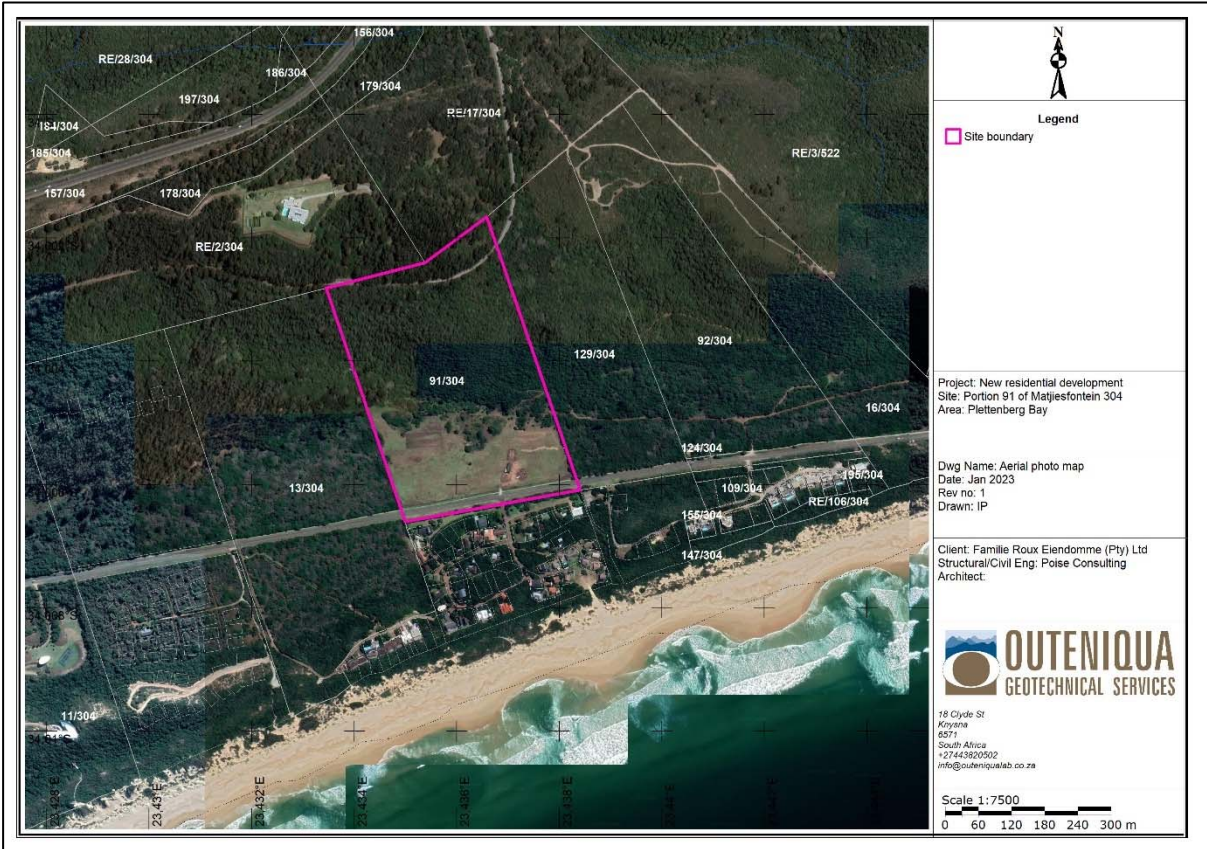


Figure 2: Aerial photo map



Figure 3: View of the southern portion of the site looking south-east



Figure 4: View of the site looking north-west

3. Methods of investigation

An initial site walk-over of the site was conducted to assess the site terrain, topographic features and any obvious geotechnical issues. This was followed by a subsurface investigation consisting of several test pits, which were excavated random fashion across the site using a TLB/Backactor. This exercise was aimed at gathering geotechnical information regarding the nature of the ground conditions (soil moisture, texture, consistency, groundwater levels, etc.). The soil profiles and photographs of the test pits were included in **Appendix 2** of this report.

Representative samples of different soil types were collected from test pits for Foundation Indicator tests and Mod/CBR/Indicator tests. The tests were performed at a SANAS-Accredited laboratory (Outeniqua Lab), in accordance with the TMH1 and ASTM methods. Details of the tests were included in **Appendix 3** of this report.

In situ dynamic cone penetrometer (DCP) tests were conducted at each test pit position from NGL to a maximum depth of 2-4m or shallower refusal. Details of the tests were included in **Appendix 4** of this report.

4. Results of the site investigation

4.1 Regional geology

The official geological mapping of the area indicated that the lower/southern portion of the site was underlain by estuarine/alluvial sand deposits of Quaternary age (yellow on map in **Figure 5**) which overlie sandstone and conglomerate of the Enon Formation (red/orange on map) of the Uitenhage Group on the northern slopes. The Enon Formation then overlies shale of the Gydo Formation and sandstone and shale of Baviaanskloof Formation which outcrop along the Keurboomstrand road to the east of the site. No major geological faults were mapped in the vicinity of the site and the risk of seismic activity was low. The geology was generally considered macro stable for development purposes with due consideration paid to local geotechnical constraints.

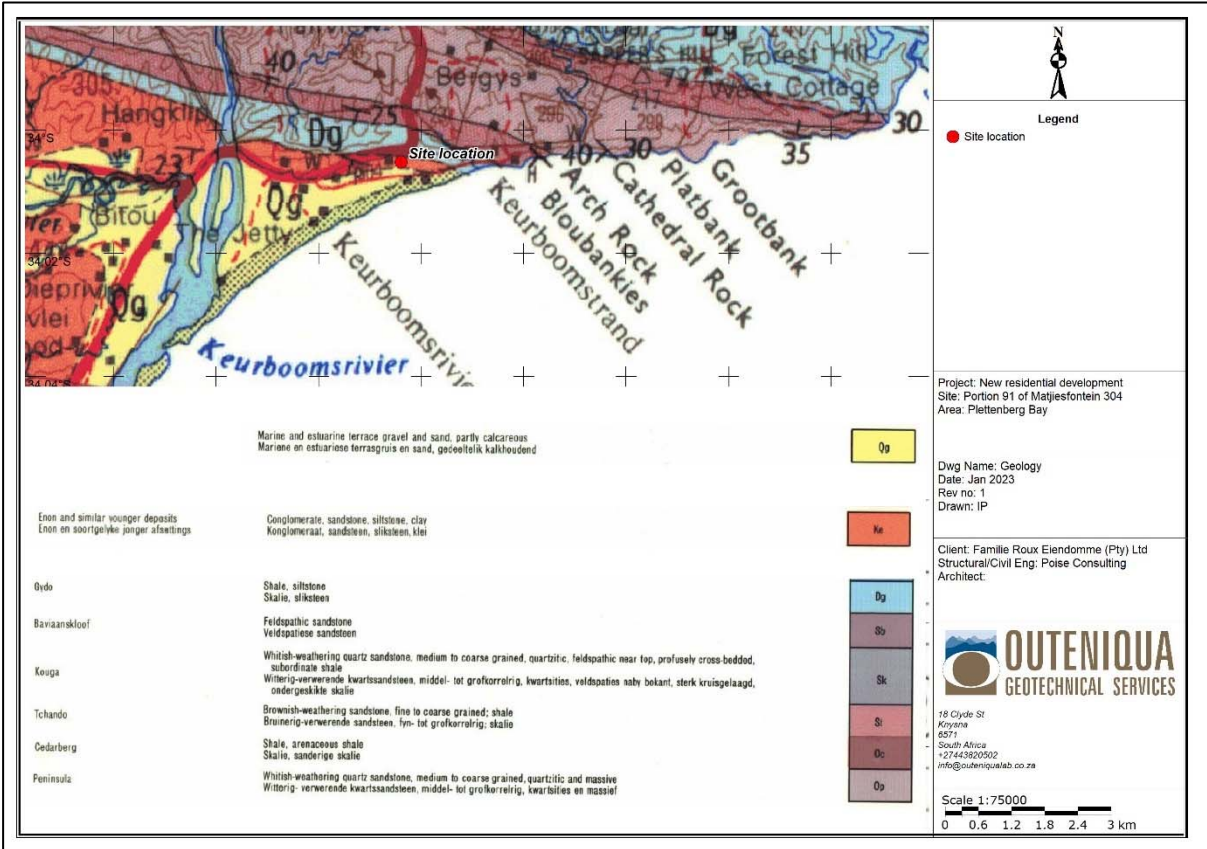


Figure 5: Geological map of site

4.2 Local soil and rock types

The soil profile was broadly consistent across the site, and dominated by estuarine sandy soil (see **Figure 6**). The profile broadly included a sporadic upper horizon of imported fill soil (disturbed or dumped soil), underlain by an insitu topsoil horizon, consisting of silty sand, roots and organic humus, which was underlain by unconsolidated to semi consolidated sand with scattered marine shell fragments. At TP5, a pedogenic calcrete hardpan layer (very soft rock) was encountered just below the topsoil horizon (see **Figure 7**). The calcrete was highly to completely weathered in places to a sandy gravel, angular cobbles and/or small boulders. A summary of the soil profiles was provided in **Table 1**.



Figure 6: Typical sandy soil types encountered in test pits



Figure 7: Calcrete hardpan layer encountered in test pit TP5

Table 1: Test pit summary - Soil horizon thickness (in mm)

Test pos. No.	Soil				Rock	Final depth of test pit	Refusal
	Imported (fill)	Transported	Pedogenic	Residual			
TP1	0-300	2000	-	-	-	2000	None
TP2	0-800	800-2600	-	-	-	2600	None
TP3	-	0-1700	-	-	-	1700	None
TP4	-	0-2600	-	-	-	1800	None
TP5	-	0-400 & 700-2500	400-700	-	-	2500	None
TP11	0-400	400-900	-	-	-	3000	None

4.3 Laboratory tests

Representative samples of different soil horizons were collected for Foundation Indicator tests in order to determine their basic geotechnical properties, estimate potential expansivity and evaluate their suitability as founding mediums. Abbreviated results of the tests were shown in **Table 2**.

The tests indicated that all the soil was dominated by fine granular soils (silty sands). All samples were non-plastic and the potential expansiveness was therefore zero. Some samples showed a measurable clay content but since the soils were non-plastic this was deemed to be from non-clay colloids, possibly including calcium carbonate. The samples tested were classified into the following categories under the Universal Soil Classification system as ML (Inorganic silts, non-plastic silts) and SM (Silty sands).

The results of the Foundation Indicator tests were summarised in **Table 2**.

Table 2: Summary of Foundation Indicator test results

Test Pit No	Sample Depth (mm)	Atterberg Limits			Particle Analysis (%)				MC*	PE**	USC ***
		PI	LL	LS	Clay	Silt	Sand	Gravel			
TP2	1500-2200	NP	NP	NP	16	21	63	0	1.5	NP	ML
TP4	800-2600	NP	NP	NP	12	13	75	0	3.2	NP	SM
TP5	700-2500	NP	NP	NP	14	42	44	0	10.7	NP	ML

* Insitu Moisture Content ** Potential Expansiveness *** Unified Soil Classification

Representative samples of insitu soils were collected for Modified AASHTO density, CBR and Road Indicator tests to determine the potential for general filling under and around structures and in roadbeds. The results of the tests were summarised in **Table 3**.

Table 3: Summary of Mod. AASHTO, CBR & Road Indicator test results

Test Pit No	Sample Depth (mm)	CBR at					Swell (%)	PI (%)	GM	MDD OMC	COLTO Class
		100 %	98%	95%	93%	90%					
TP2	500-2000	12	10	9	8	6	0	NP	1.4	1669/11.6	G8
TP3	0-700	20	14	8	6	3	0	NP	1.0	1751/12.2	G9
TP4	800-2600	17	14	11	9	7	0	NP	1.22	1614/11.2	G8

The test results indicated that the insitu material was dominated by silty fine sand with marginal strength properties but was generally suitable as bulk filling under and around structures or for road subgrade fill. Recommendations were given in **Chapter 6**.

4.4 Insitu tests

In situ penetration tests (DCP) indicated significant variation in the consistency of the soil in the upper 0.7m of the profile, but consistently dense conditions below this level.

Table 4: Summary of DCP tests

Test Pos No	0-1m			1-2m			2-3m			3-4m		
	DN	Con	ϕ°	DN	Con	ϕ°	DN	Con	ϕ°	DN	Con	ϕ°
1	40	L	28	29	MD	30	n/a	-	-	n/a	-	-
2	25	MD	32	21	MD	32	n/a	-	-	n/a	-	-
3	33	MD	30	31	MD	30	n/a	-	-	n/a	-	-
4	34	MD	30	26	MD	32	20	MD	33	11	D	
5	40	L	28	10	D	36	n/a	-	-	n/a	-	-
6	45	L	28	22	MD	32	n/a	-	-	n/a	-	-
7	27	MD	32	24	MD	32	11	D		23	MD	32
8	42	L	28	26	MD	32	20	MD	33	16	D	34
9	52	L	28	25	MD	32	21	MD	32	23	MD	32
10	38	MD	30	21	MD	32	14	D	35	16	D	34

*DN – Max penetration rate Con - Consistency

DCP tests indicated a general improvement in density and bearing capacity with increasing

depth with some minor variations. The tests confirmed that shallow foundations would be generally suitable but good compaction would be required to mitigate settlement, particularly in the foundation influence zone within a depth range of up to 2m below NGL.

5. Geotechnical assessment

5.1 Site classification

The site was mapped according to the site class designations provided in SANS10400-H (refer to **Table 5**). Due to the broadly consistent conditions observed in the investigation, the majority of the proposed development footprint area was mapped as a single geotechnical terrain with the site class designation of **S1** (potentially compressible sandy soils). Minor superficial deposits of uncontrolled fill (**P**) were also mapped as indicated in **Figure 8**.

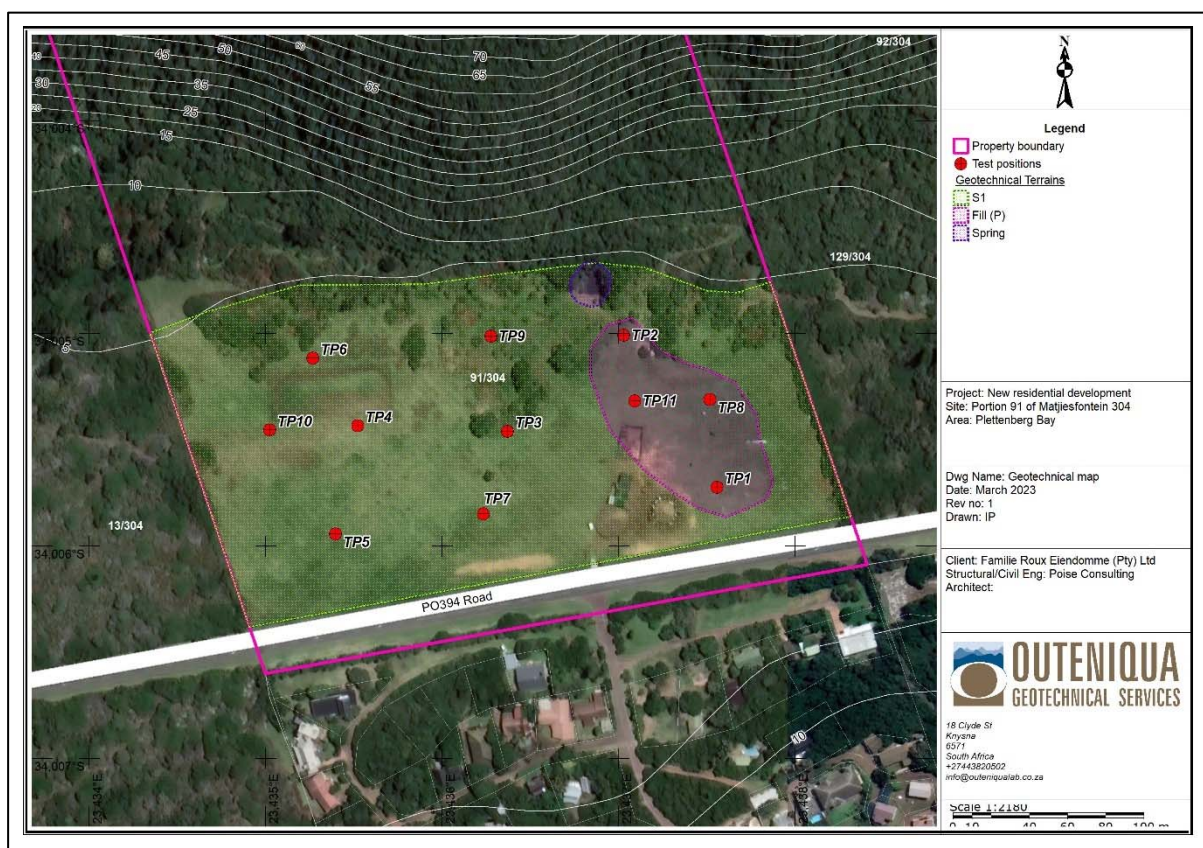


Figure 8: Geotechnical map

Table 4: SANS 10400-H Geotechnical site class designations

1	2	3	4	5
Typical founding material	Nature of founding material	Expected range of total soil movements mm	Assumed differential movement % of total	Site class designation
Rock (excluding mud rocks which might exhibit swelling to some depth)	Stable	Negligible	–	R
Fine-grained soils with moderate to very high plasticity (clays, silty clays, clayey silts and sandy clays)	Expansive soils	< 7,5 7,5 to 15 15 to 30 > 30	50 50 50 50	H H1 H2 H3
Silty sands, clayey sands, sands, sandy and gravelly soils	Compressible and potentially collapsible soils	< 5 5 to 10 > 10	75 75 75	C C1 C2
Fine-grained soils (clayey silts and clayey sands of low plasticity), sands, sandy and gravelly soils	Compressible soils	< 10 10 to 20 > 20	50 50 50	S S1 S2
Contaminated soils ^a , controlled fill, dolomite land, landslip, landfill, marshy areas, mine waste fill, mining subsidence reclaimed areas, uncontrolled fill, very soft silts/silty clays	Variable	Variable	–	P ^b

5.2 Bearing capacity and settlement of structures

Observations made during the site investigations and analysis of test results indicated that the natural soils at normal shallow levels (0.5-1m) was dominated by potentially compressible fine sand. The soil would require improvement (compaction) to safely support type 1 residential structures on conventional shallow spread foundations with typical bearing pressures of up to 150kPa. Beyond this maximum typical load, the depth of improvement or type of foundation would require further consideration.

Other geotechnical constraints which could affect earthworks or foundations, such as uncontrolled fill, surface water bodies and ground water were also identified. Earthworks and foundation design recommendations were provided in **Chapter 6**.

5.3 Heave

The soil profile was not expected to display any significant expansivity and no special measures would be required to cater for heave.

5.4 Groundwater and site drainage

The fine sandy soil conditions generally had moderate permeability and drainage characteristics, but surface water was expected to accumulate temporarily after heavy rainfall events. A surface water body, fed by a perennial spring, was also identified at the base of the slope on the eastern side of the site. Groundwater was identified in test pits on the southern (lower) side of the site (TP1 & TP5) at an average depth of 2m. Seepage and run-off from the slopes to the north were therefore expected to have an influence on the engineering design. Groundwater was also expected to affect deep excavations (>1.5m below NGL) in some areas.

5.5 Slopes

No slope stability problems were observed on the steep slopes above (to the north) of the proposed development area. The maximum gradient of the slopes was estimated from contour data at 1:1.5. The slopes were covered in dense vegetation and generally inaccessible for detailed inspection but according to the geological map, the slopes were underlain by dense conglomerate and sandstone of the Enon Formation, which was well exposed in near-vertical road cuttings to the northwest of the site. The slopes had been enjoying a state of general stability for many years and this was deemed to be due to the stable underlying geology and was therefore not considered to present a significant risk to the site.

5.6 Excavations

All excavations to 2m were provisionally classified as "Soft" in terms of SABS1200D, and easily excavatable by hand or with light machinery (TLB). Sidewalls of temporary excavations (trenches) were expected to be highly unstable, even for short periods, due to the loose sandy soil types.

5.7 Natural construction materials

The sandy soils that were encountered in test pits were classified as G8-9 and were deemed to be potentially suitable as general structural fill material under foundations and floors or behind retaining walls, when placed and compacted to the engineer's specifications.

6. Recommendations

The following recommendations are based on limited information gained from the site investigation and although the confidence in the information is high, significant variation is likely to occur between information points. All geotechnical information should be verified during construction and any significant variations should be brought to the attention of the geotechnical engineer for comment or further recommendations. It is recommended that the structural & civil engineers discuss their designs with the geotechnical engineer to ensure that the designs are compatible with the expected geotechnical conditions.

6.1 Earthworks and structural foundations

Earthworks should be designed and constructed in accordance with SABS 1200D and/or any site-specific specifications provided by the civil engineer. Foundations should be designed and constructed in accordance with SANS 10400-H or as specified by the structural engineer.

To clear and prepare site for earthworks and construction, it was recommended that at least 150mm of topsoil and vegetation cover be removed from the footprint area. Large roots be grubbed and platform levels established by cutting and/or filling with insitu soil obtained from site. Bulk fill should be compacted to minimum 93%MDD. Low retaining walls may be required in some areas, depending on site levels. The insitu sandy soils were generally suitable for use as general fill on platforms, in roadbeds and as trench backfill. Any organic matter or unsuitable soil should be removed from potential fill material.

Unsuitable ground conditions exposed during earthworks should be referred to the engineer for further investigation and consideration on appropriate action.

The recommended foundation system for the proposed single/double storey residential structures included the following:

- a. RC strips/bases – clear and level site to PL, excavate trenches to PL-1m, wet and compact base of trench with 6 passes of mechanical rammer, such that DCP penetrates at less than 30mm/blow to a depth of 1m below the base of the excavation, backfill the trench to PL-0.7m (recommended final founding level) in layers with compacted sand ex-insitu to 100%MDD or <20mm/blow of DCP. Limit bearing pressures to max 150kPa. Alternatively, excavate trenches to PL-0.7m, compact base of trench such that DCP penetrates at less than 30mm/blow and limit bearing pressures to 100kPa.
- b. Raft foundations on a compacted insitu platform – excavate ~0.6m of insitu soils below entire platform area, compact base of excavation with roller, replace compacted soil in layers back up to platform level such that DCP penetrates at <30mm/blow, construct light raft foundation with max bearing pressures of 75kPa.

Additional measures can be considered for heavier structures.

Regular supervision by the structural engineer was highly recommended to ensure suitable founding conditions.

6.2 Site drainage

The design and construction of storm water drainage should be carried out in accordance with SABS 1200LE, COLTO, The Red Book or other applicable standards, as determined by the civil engineer.

Consideration should be paid to stormwater drainage due to the low gradient on the site and the likelihood of stormwater accumulating on surface after heavy downpours. Stormwater from roofs can generally be handled in gutters, downpipes and open channels or underground pipes, with suitable discharge locations on the southern side of the site. A well designed road layout can assist in management of stormwater run-off from site, with minor flood events being accommodated within the road prism with raised barrier kerbs and/or side channels.

Allowances should be made for stormwater handling from slopes above the site (including continual seepage at/near spring area).

6.3 Roads

It is recommended that road layerworks, including G4-G6 subbase and G1-G4 base layers (for asphalt-sealed roads) be imported from local commercial quarries. The insitu sandy soil can be used for roadbed and SSG layerworks in lightly trafficked internal estate roads.

7. Conclusions

The investigations have indicated that the site was potentially suitable for the proposed development but there were some moderate geotechnical constraints which required consideration in the structural design. Some preliminary recommendations were provided but all geotechnical information should be verified during construction.

Appendix 1

Maps



Legend

 Site location

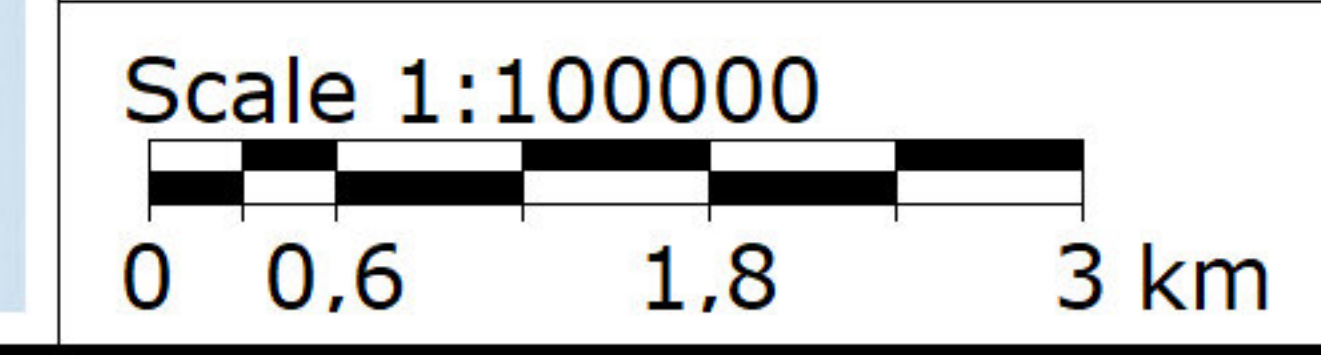
Project: New residential development
 Site: Portion 91 of Matjiesfontein 304
 Area: Plettenberg Bay

Dwg Name: Locality map
 Date: Jan 2023
 Rev no: 1
 Drawn: IP

Client: Familie Roux Eiendomme (Pty) Ltd
 Structural/Civil Eng: Poise Consulting
 Architect:



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Legend

Site boundary

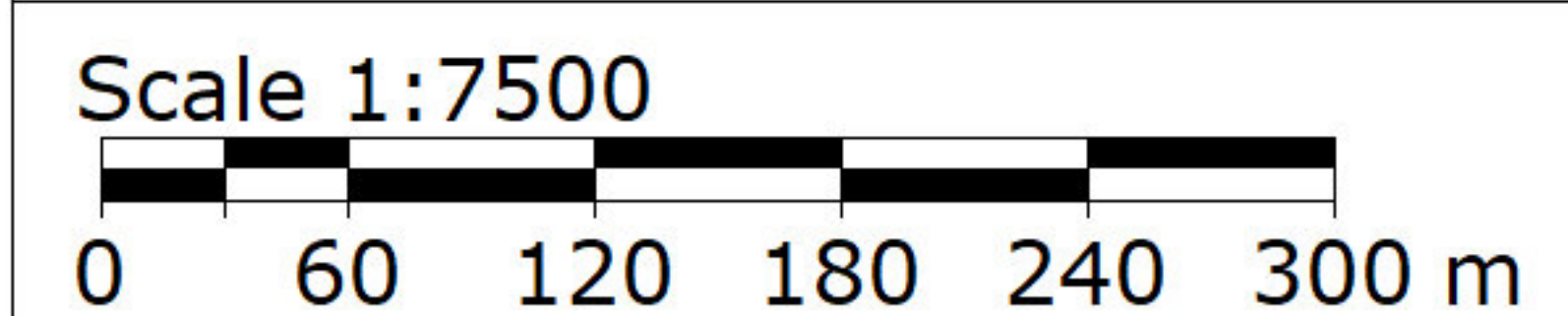
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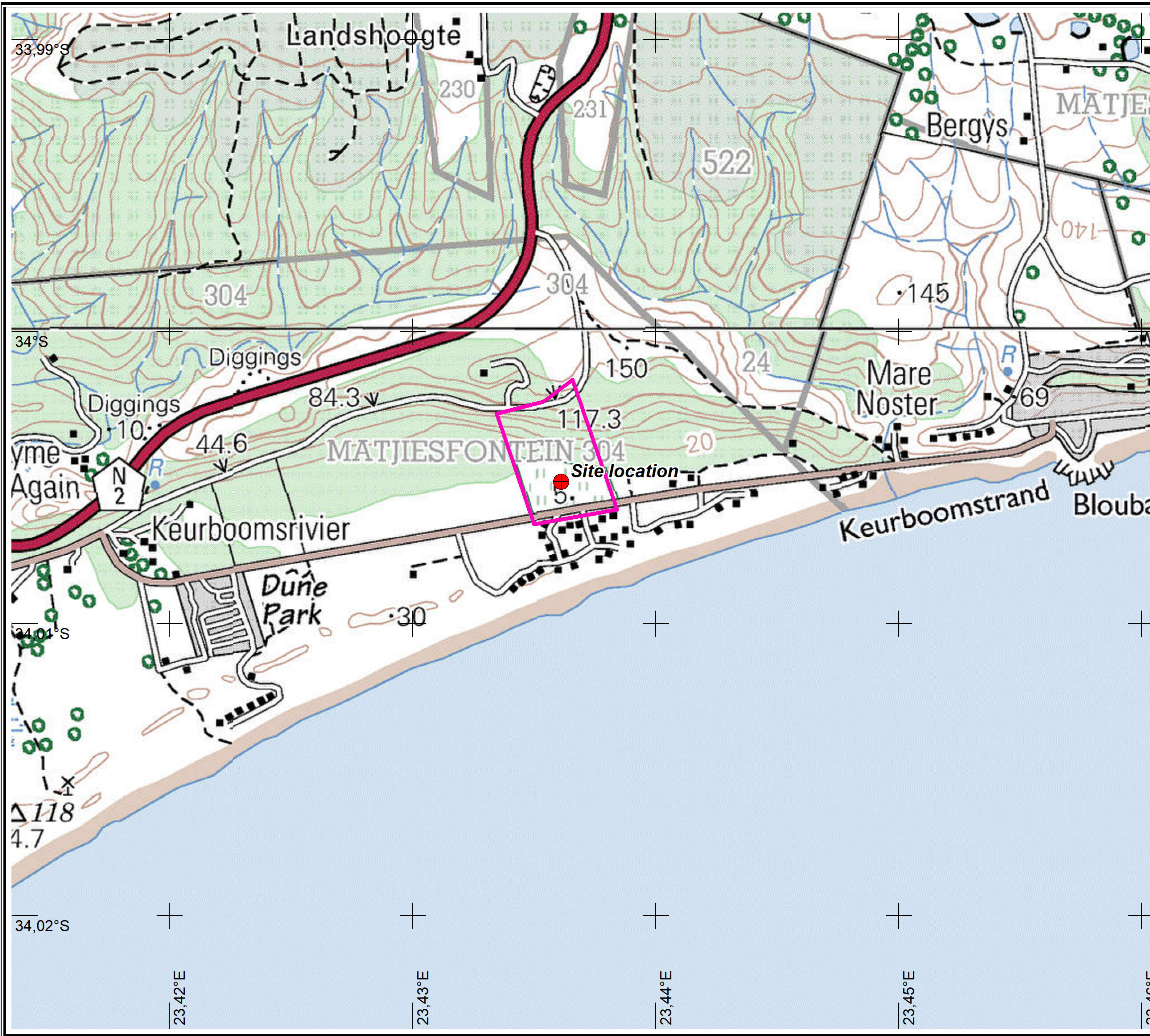
Dwg Name: Aerial photo map
 Date: Jan 2023
 Rev no: 1
 Drawn: IP

Client: Familie Roux Eiendomme (Pty) Ltd
 Structural/Civil Eng: Poise Consulting
 Architect:



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Legend

- Site boundary
- Site location

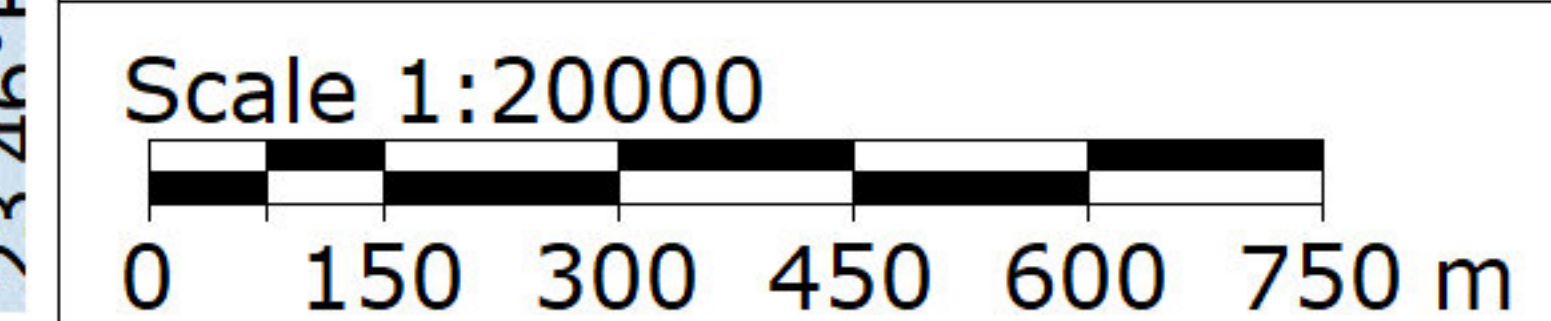
Project: New residential development
 Site: Portion 91 of Matjiesfontein 304
 Area: Plettenberg Bay

Dwg Name: Topographical map
 Date: Jan 2023
 Rev no: 1
 Drawn: IP

Client: Familie Roux Eiendomme (Pty) Ltd
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33,99°S

34°S

34,01°S

34,02°S

23,42°E

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23,46°E



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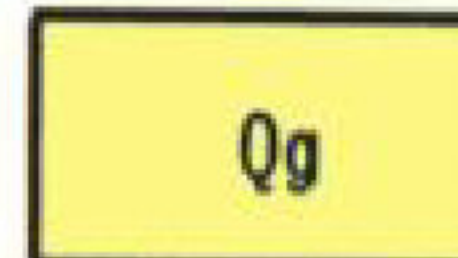
 Site location

Project: New residential development
 Site: Portion 91 of Matjiesfontein 304
 Area: Plettenberg Bay

Dwg Name: Geology
 Date: Jan 2023
 Rev no: 1
 Drawn: IP

Client: Familie Roux Eiendomme (Pty) Ltd
 Structural/Civil Eng: Poise Consulting
 Architect:

Marine and estuarine terrace gravel and sand, partly calcareous
 Mariene en estuariese terrasgruis en sand, gedeeltelik kalkhoudend



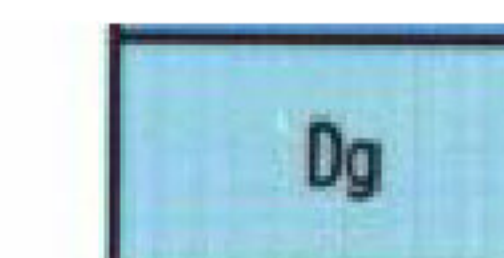
Enon and similar younger deposits
 Enon en soortgelyke jonger afsettings

Conglomerate, sandstone, siltstone, clay
 Konglomeraat, sandsteen, sliiksteen, klei



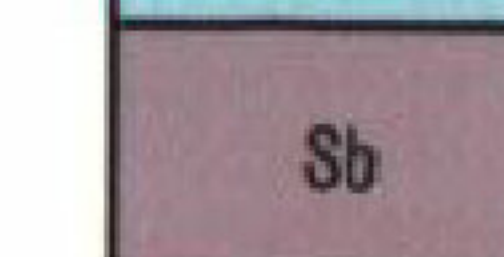
Gydo

Shale, siltstone
 Skalie, sliiksteen



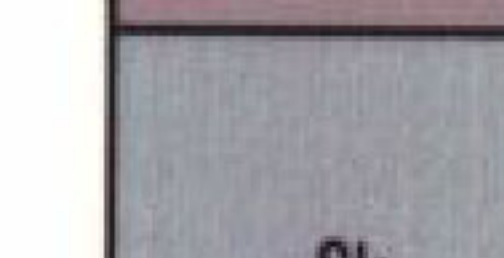
Baviaanskloof

Feldspathic sandstone
 Veldspatiese sandsteen



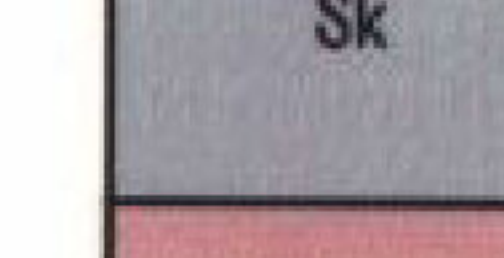
Kouga

Whitish-weathering quartz sandstone, medium to coarse grained, quartzitic, feldspathic near top, profusely cross-bedded, subordinate shale
 Witterig-verwerende kwartssandsteen, middel- tot grofkorrelrig, kwartsities, veldspaties naby bokant, sterk kruisgelaagd, ondergeskikte skalie



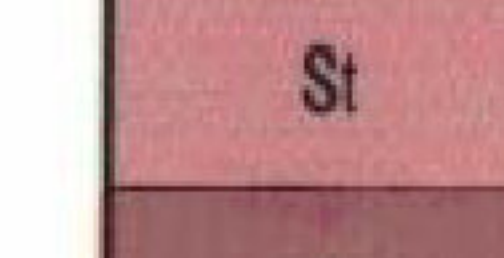
Tchando

Brownish-weathering sandstone, fine to coarse grained; shale
 Bruinerig-verwerende sandsteen, fyn- tot grofkorrelrig; skalie



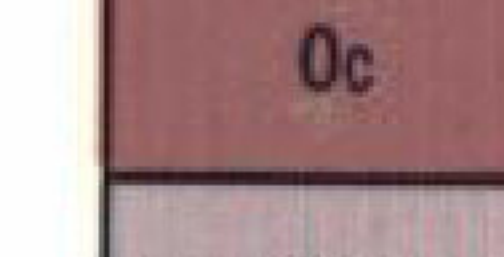
Cedarberg

Shale, arenaceous shale
 Skalie, sanderige skalie

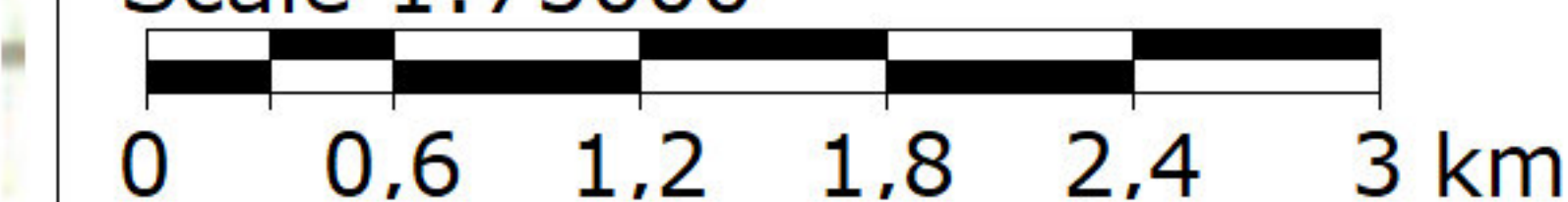


Peninsula

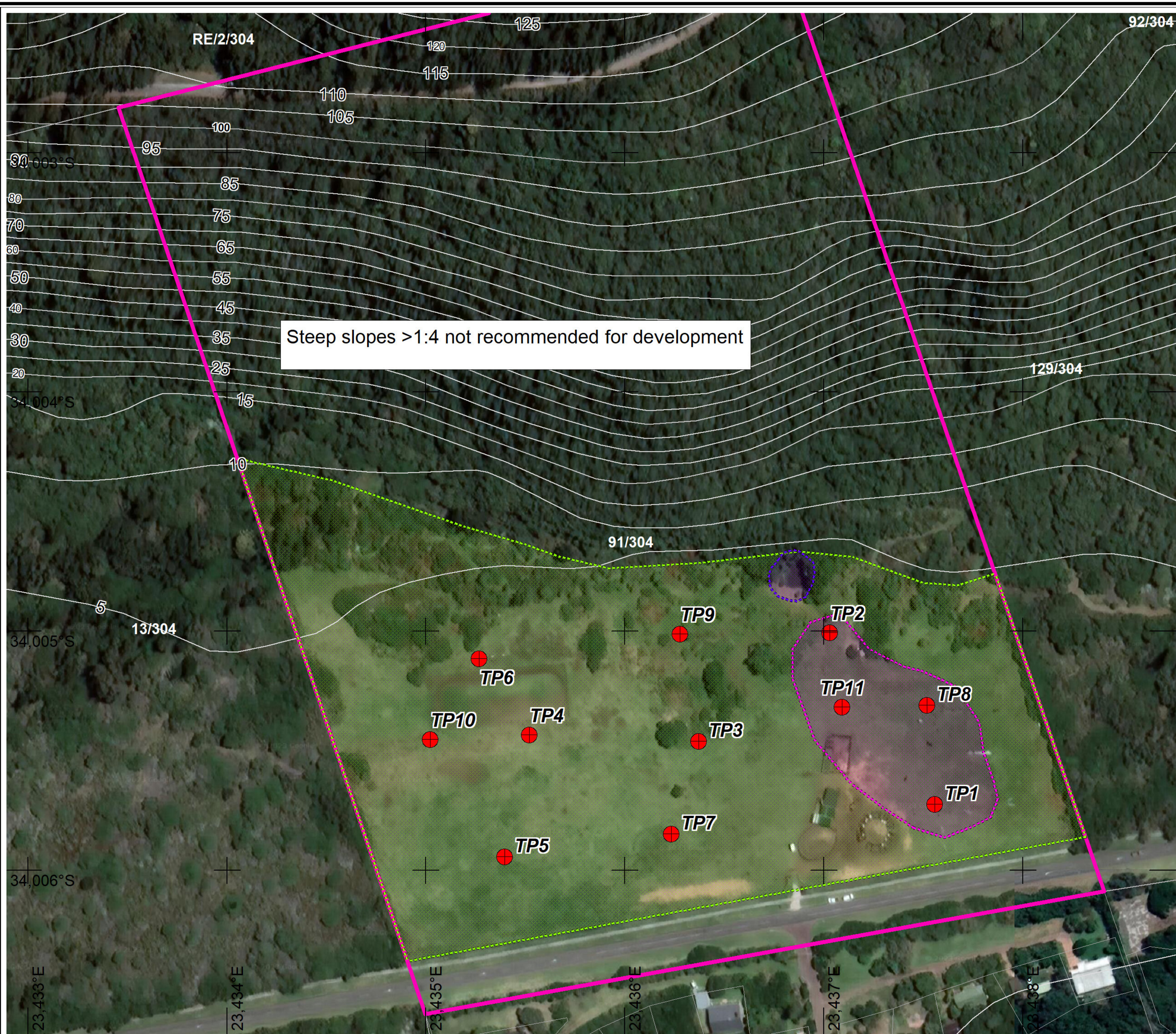
Whitish-weathering quartz sandstone, medium to coarse grained, quartzitic and massive
 Witterig- verwerende kwartssandsteen, middel- tot grofkorrelrig, kwartsities en massief



Scale 1:75000








18 Clyde St
 Knysna
 6571
 South Africa
 +27443820502
 info@outeniqua.co.za



Steep slopes > 1:4 not recommended for development



Legend

-  Property boundary
-  Test positions
- Geotechnical Terrains**
-  S1
-  Fill (P)
-  Spring

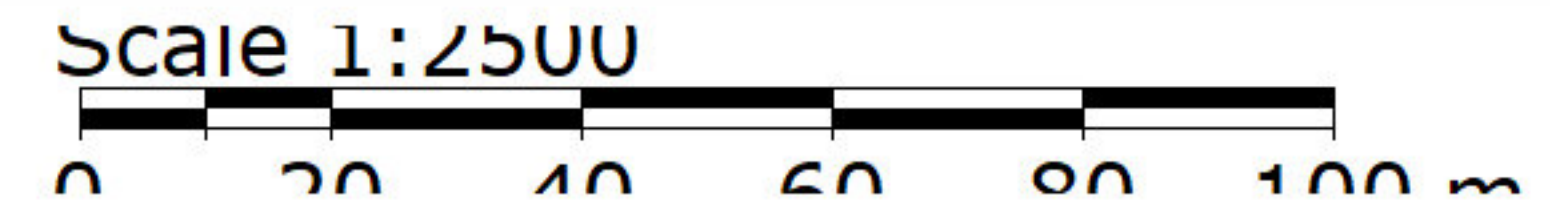
Project: New residential development
 Site: Portion 91 of Matjiesfontein 304
 Area: Plettenberg Bay

Dwg Name: Geotechnical map
 Date: March 2023
 Rev no: 1
 Drawn: IP

Client: Familie Roux Eiendomme (Pty) Ltd
 Structural/Civil Eng: Poise Consulting
 Architect:



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 Knysna
 6571
 South Africa
 +27443820502
 info@outeniqua.co.za



Appendix 2

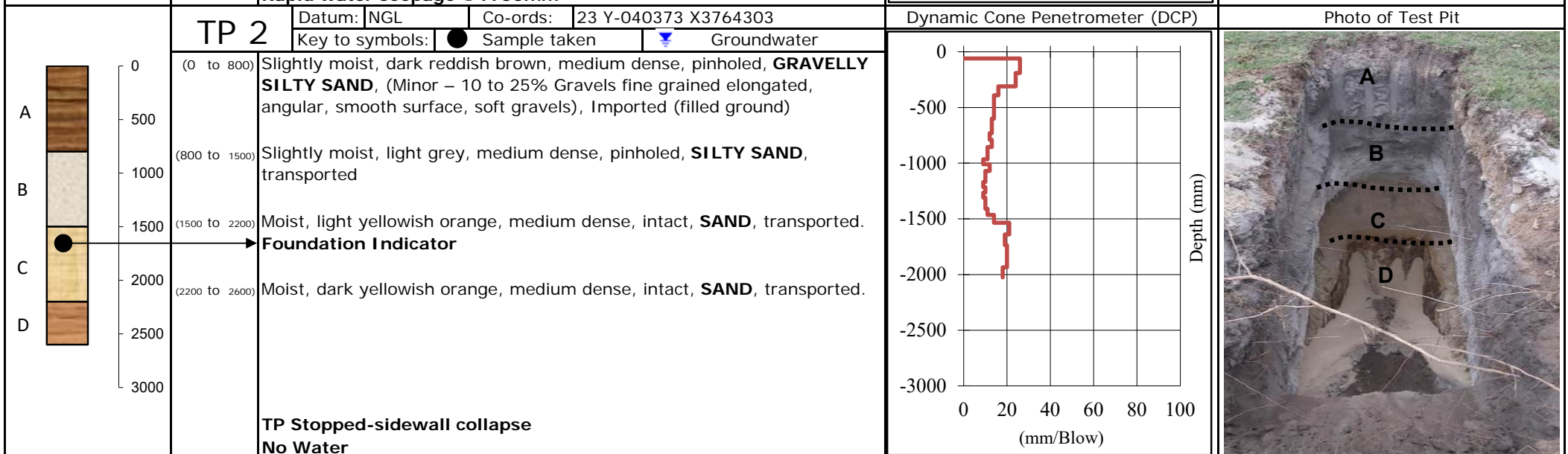
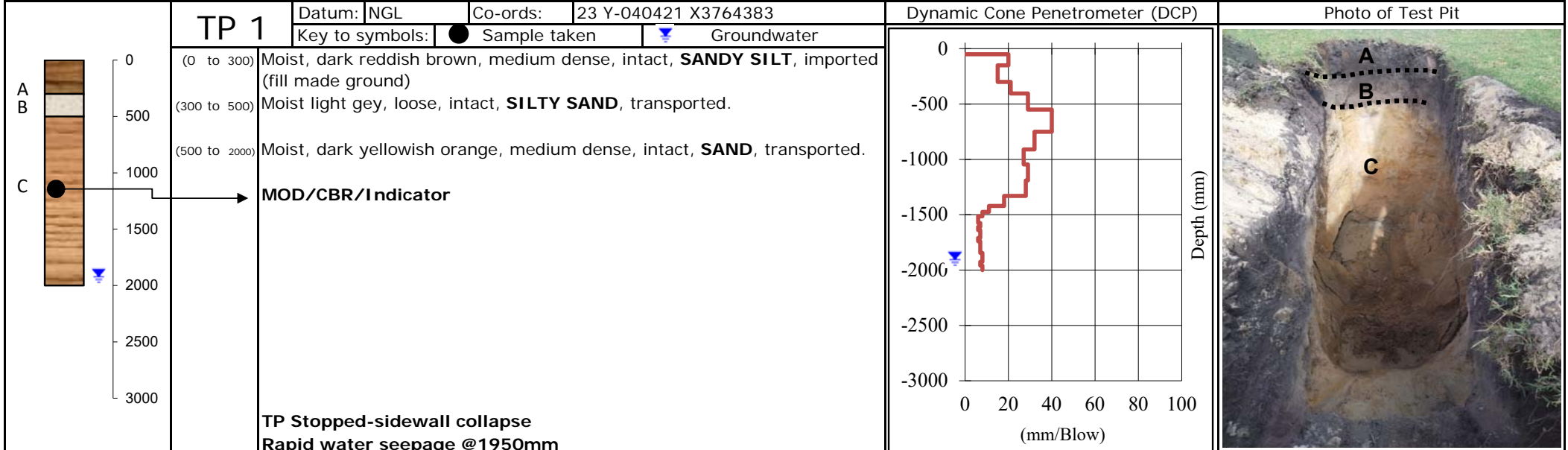
Test pit profiles



OUTENIQUA GEOTECHNICAL SERVICES

Geotechnical Soil Profile

Client:	Poise Consulting Engineers
Project:	Portion 91 of Matjiesfontien 304
Area:	Keurboomstrand
Date:	01.02.2023
Excavator:	TLB

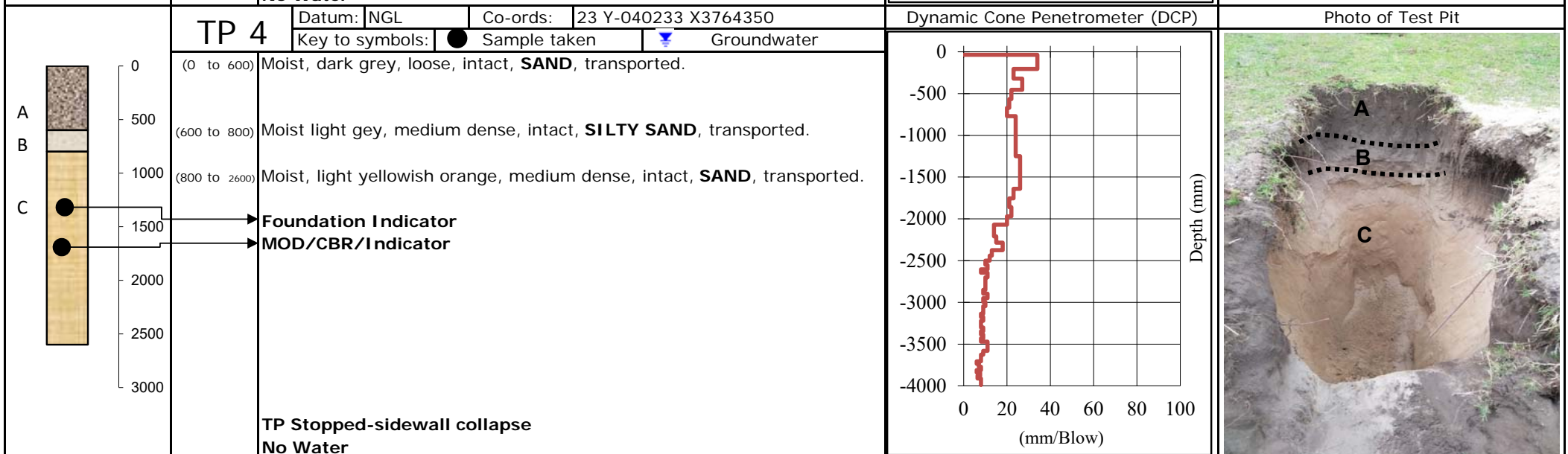
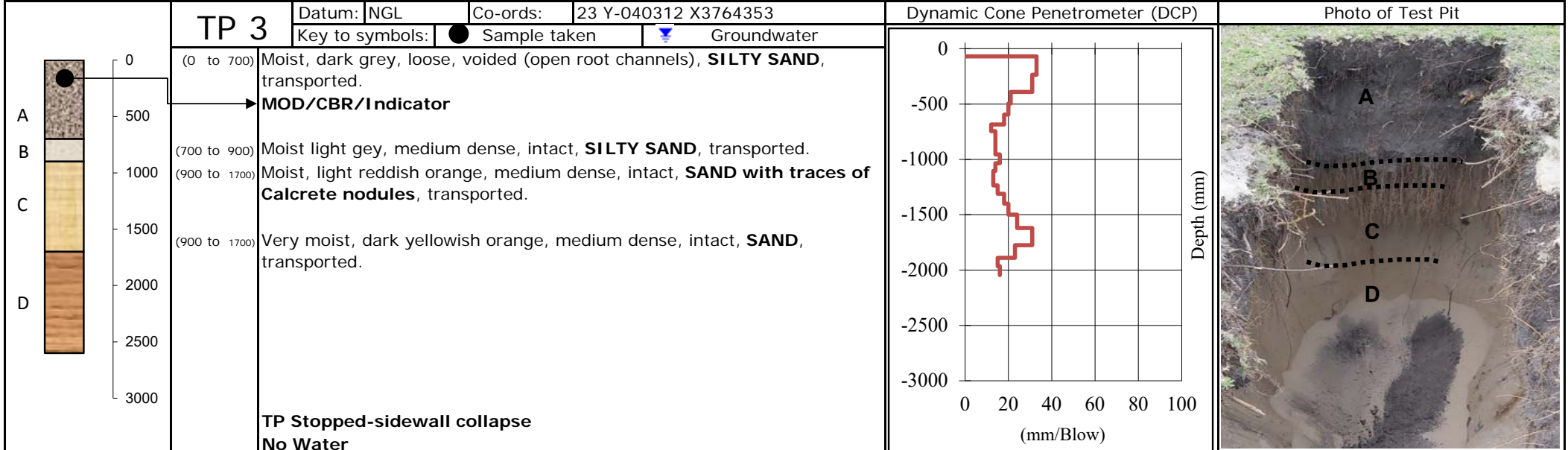




OUTENIQUA GEOTECHNICAL SERVICES

Geotechnical Soil Profile

Client:	Poise Consulting Engineers
Project:	Portion 91 of Matjiesfontien 304
Area:	Keurboomstrand
Date:	01.02.2023
Excavator:	TLB

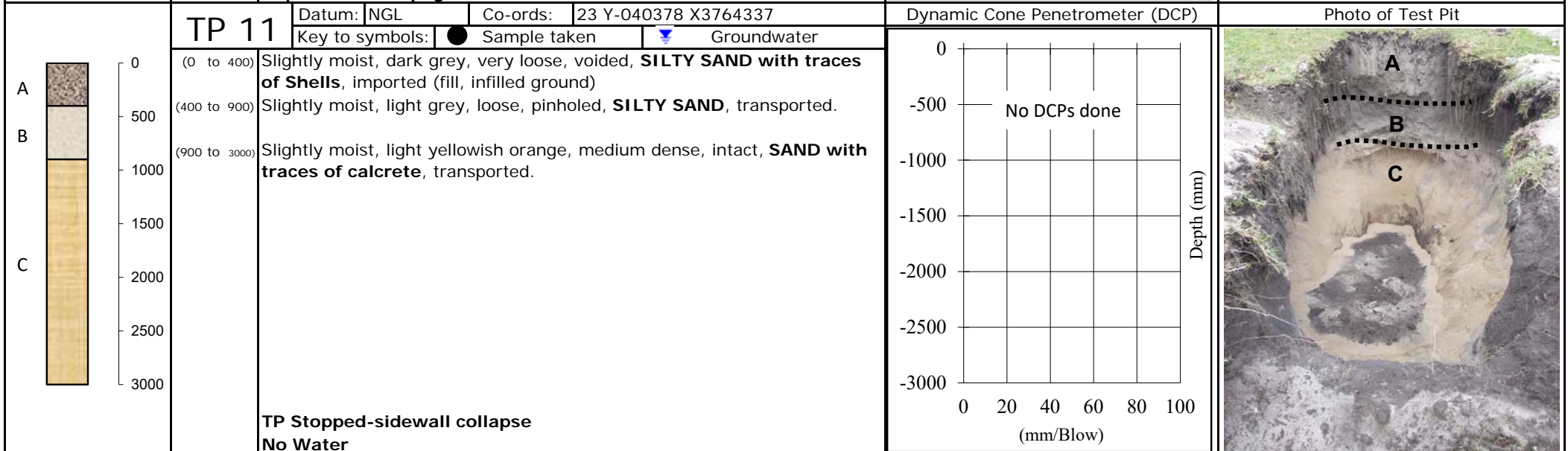
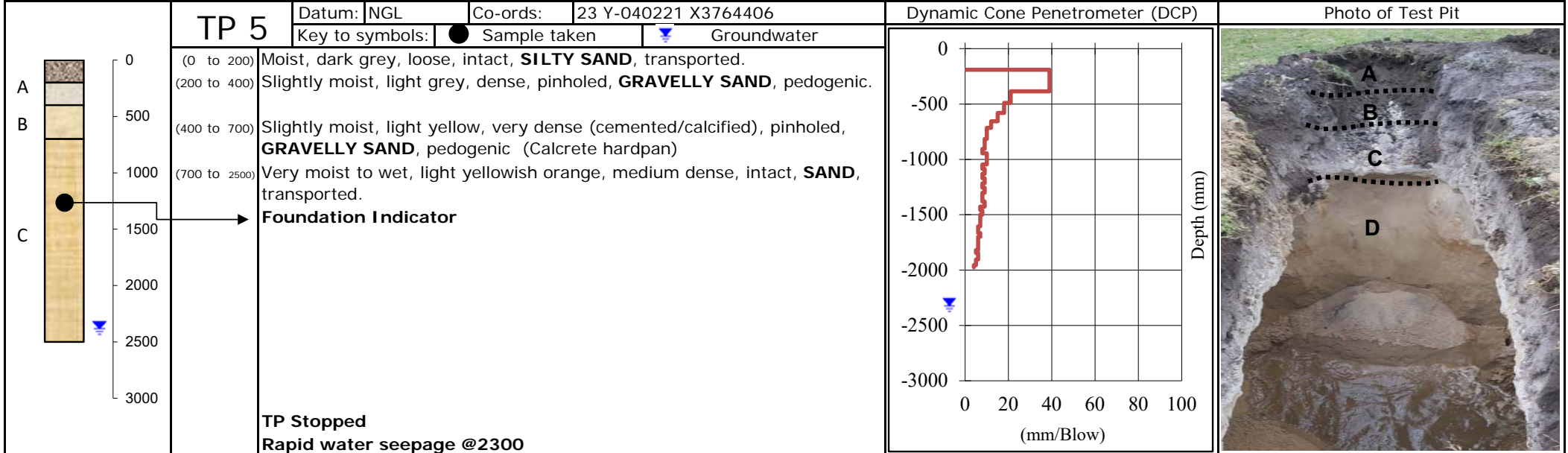




OUTENIQUA GEOTECHNICAL SERVICES

Geotechnical Soil Profile

Client:	Poise Consulting Engineers
Project:	Portion 91 of Matjiesfontien 304
Area:	Keurboomstrand
Date:	01.02.2023
Excavator:	TLB



Appendix 3

Lab test data



OUTENIQUA LAB (Pty) Ltd.

Registration No. 95/07742/07

Materials Testing Laboratory

6 Mirrorball Street, George : PO Box 3186, George Industria, 6536

Tel: 044 8743274 : Fax: 044 8745779 : e-mail: llewelyn@outeniqualab.co.za

R-FIND-1-6

Jan-22



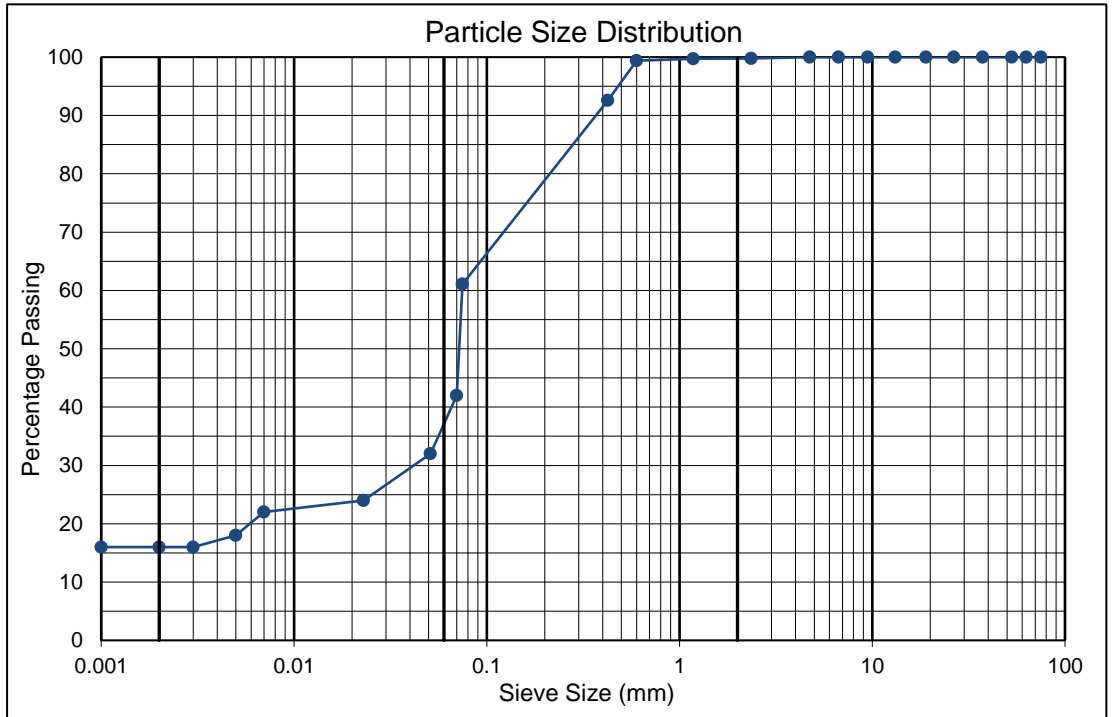
T0347

Customer :	Outeniqua Geotechnical Services	Project :	Portion 91 of Matjiesfontein 304 - Keurboomstrand
	P O Box 964	Date Received :	08/02/2023
Attention :	Knysna	Date Reported :	06/03/2023
	6570	Req. Number :	0322/22
	Iain Paton	No. of Pages :	1/3

TEST REPORT FOUNDATION INDICATOR - (ASTM Method D422)

Sample Position (SV)	TP2	
Depth (mm):	1500-2200	
Sample No.:	85881	
Materials Description	Source	
	Colour	In-situ
	Soil Type	Dark Yellowish Orange
	Classification	Sandy Silt Existing

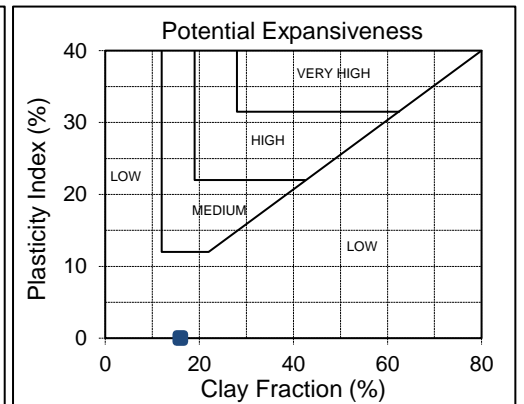
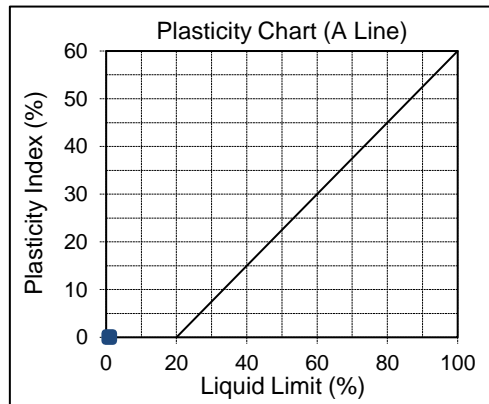
75.0mm	100
63.0mm	100
53.0mm	100
37.5mm	100
26.5mm	100
19mm	100
13.2mm	100
9.5mm	100
6.7mm	100
4.75mm	100
2.36mm	100
1.18mm	100
0.6mm	99
0.425mm	93
0.075mm	61
0.07mm	42
0.051mm	32
0.023mm	24
0.007mm	22
0.005mm	18
0.003mm	16
0.002mm	16
0.001mm	16



Liquid Limit (%)	NP
Plasticity Index (%)	NP
Linear Shrinkage (%)	NP
Moisture Content (%)	1.5

% Clay	16
% Silt	21
% Sand	63
% Gravel	0

Unified Soil Classification	ML
AASHTO Soil Classification	A-4



• Specimen delivered to Outeniqua Lab in good order.

Ruan Lesch
Technical Signatory
For Outeniqua Lab (Pty) Ltd.

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Tel: 044 8743274 : Fax: 044 8745779 : e-mail: llewelyn@outeniqualab.co.za

R-FIND-1-6

Jan-22



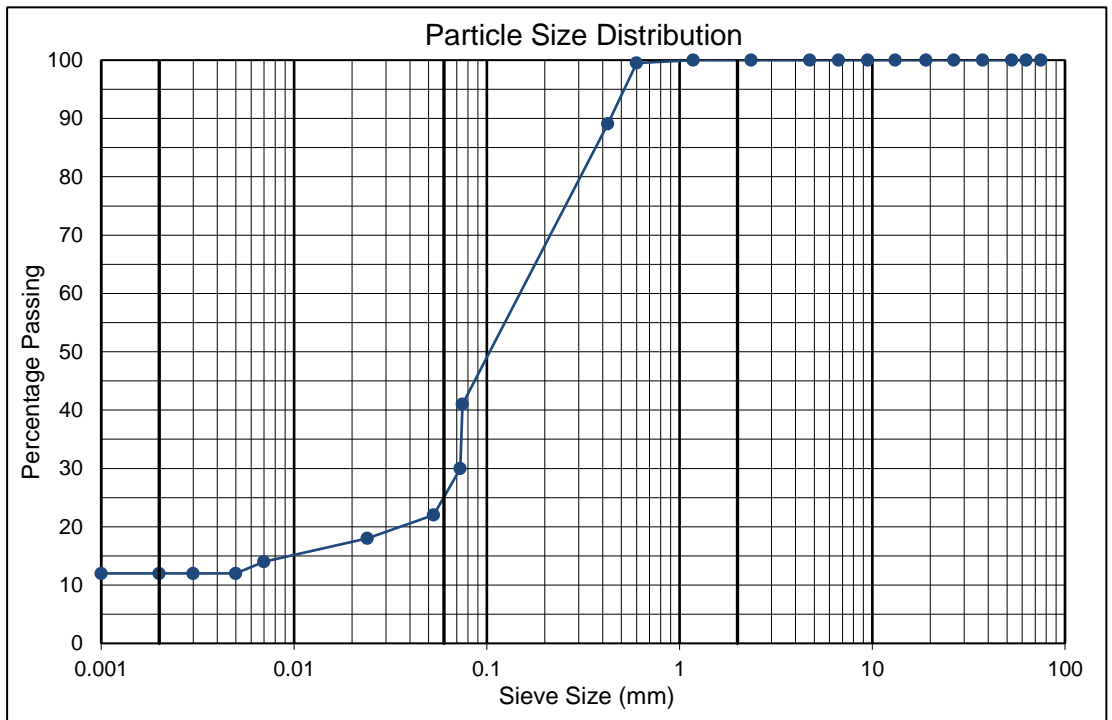
T0347

Customer :	Outeniqua Geotechnical Services	Project :	Portion 91 of Matjiesfontein 304 - Keurboomstrand
	P O Box 964	Date Received :	08/02/2023
Attention :	Knysna	Date Reported :	06/03/2023
	6570	Req. Number :	0322/22
	Iain Paton	No. of Pages :	2/3

TEST REPORT FOUNDATION INDICATOR - (ASTM Method D422)

Sample Position (SV)	TP4	
Depth (mm):	800-2600	
Sample No.:	85883	
Materials Description	Source	In-situ
	Colour	Light Yellowish Orange
	Soil Type	Sand
	Classification	Existing

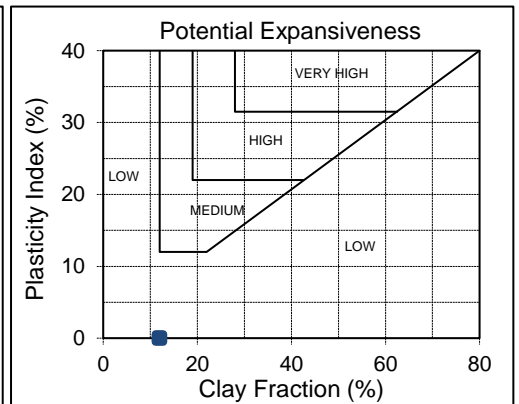
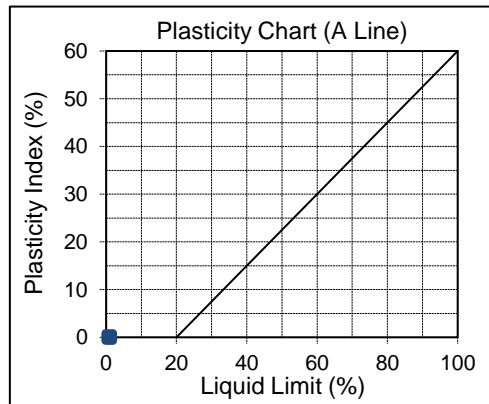
75.0mm	100
63.0mm	100
53.0mm	100
37.5mm	100
26.5mm	100
19mm	100
13.2mm	100
9.5mm	100
6.7mm	100
4.75mm	100
2.36mm	100
1.18mm	100
0.6mm	100
0.425mm	89
0.075mm	41
0.073mm	30
0.053mm	22
0.024mm	18
0.007mm	14
0.005mm	12
0.003mm	12
0.002mm	12
0.001mm	12



Liquid Limit (%)	NP
Plasticity Index (%)	NP
Linear Shrinkage (%)	NP
Moisture Content (%)	3.2

% Clay	12
% Silt	13
% Sand	75
% Gravel	0

Unified Soil Classification	SM
AASHTO Soil Classification	A-4



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Ruan Lesch
Technical Signatory
For Outeniqua Lab (Pty) Ltd.

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Materials Testing Laboratory

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Tel: 044 8743274 : Fax: 044 8745779 : e-mail: llewelyn@outeniqualab.co.za

R-FIND-1-6

Jan-22



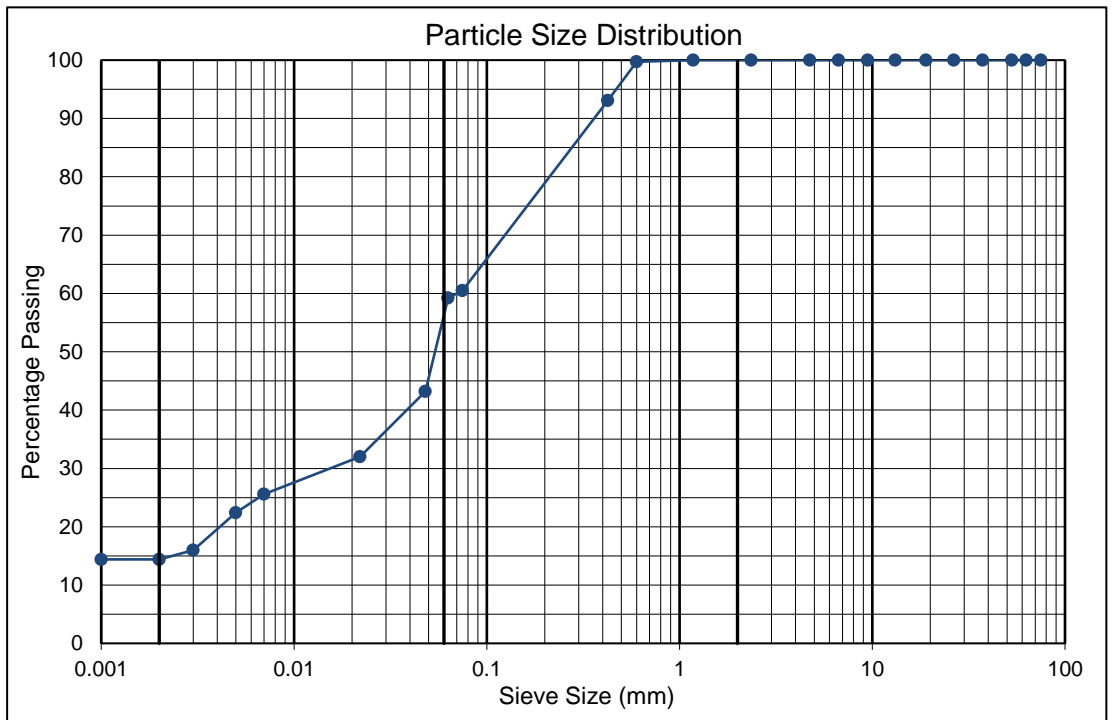
T0347

Customer :	Outeniqua Geotechnical Services	Project :	Portion 91 of Matjiesfontein 304 - Keurboomstrand
	P O Box 964	Date Received :	08/02/2023
Attention :	Knysna	Date Reported :	06/03/2023
	6570	Req. Number :	0322/22
	Iain Paton	No. of Pages :	3/3

TEST REPORT FOUNDATION INDICATOR - (ASTM Method D422)

Sample Position (SV)	TP4
Depth (mm):	700-2500
Sample No.:	85884
Materials Description	In-situ Light Yellowish Orange to Light Grey Sandy Silt Existing

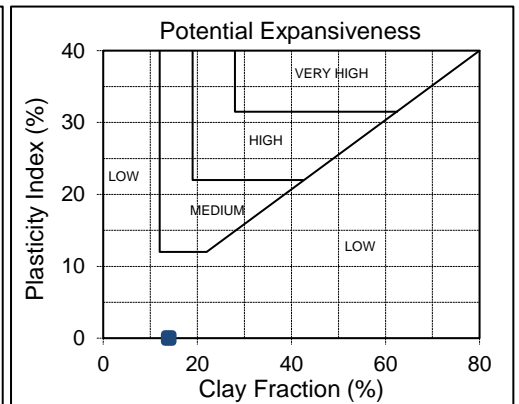
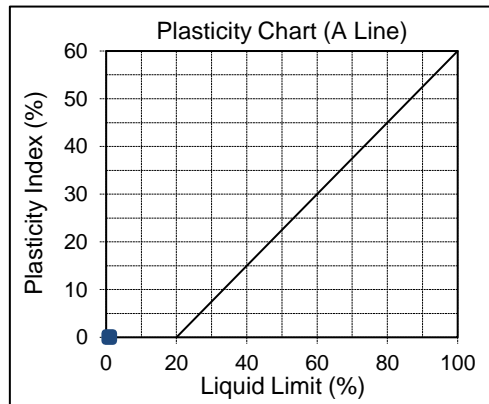
75.0mm	100
63.0mm	100
53.0mm	100
37.5mm	100
26.5mm	100
19mm	100
13.2mm	100
9.5mm	100
6.7mm	100
4.75mm	100
2.36mm	100
1.18mm	100
0.6mm	100
0.425mm	93
0.075mm	61
0.063mm	59
0.048mm	43
0.022mm	32
0.007mm	26
0.005mm	22
0.003mm	16
0.002mm	14
0.001mm	14



Liquid Limit (%)	NP
Plasticity Index (%)	NP
Linear Shrinkage (%)	NP
Moisture Content (%)	10.7

% Clay	14
% Silt	42
% Sand	44
% Gravel	0

Unified Soil Classification	ML
AASHTO Soil Classification	A-4



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Ruan Lesch
Technical Signatory
For Outeniqua Lab (Pty) Ltd.

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Customer :	Outeniqua Geotechnical Services	Project :	Portion 91 of Matjiesfontein 304 - Keurboomstrand
	P O Box 964	Date Received :	08/02/2023
	Knysna	Date Reported :	22/02/2023
	6570	Req. Number :	0322/23
Attention :	Iain Paton	No. of Pages :	1/3

TEST REPORT CALIFORNIA BEARING RATIO

Sample Position (SV)		TP1	COLTO:				
Depth (mm)		500-2000	G8 SSG				
Sample No		85880					
Materials Description	Source	In-situ					
	Colour	Dark Yellowish Orange					
	Soil Type	Sand					
	Classification	Proposed (G7)					
Material Indicators - (SANS 3001 Method GR1)							
Percentage Passing	75 mm	100		Opinion			
	63 mm	100					
	50 mm	100					
	37.5 mm	100					
	28 mm	100					
	20 mm	100					
	14 mm	100					
	5 mm	100					
	2 mm	100					
	0.425 mm	56					
0.075 mm	3.4						
Material Indicators - (SANS 3001 Method PR5)							
Grading Modulus *		1.40	0.75 - 2.70	✓			
Coarse Sand Soil-Mortar (%)		43					
Atterberg Limits - (SANS 3001 Method GR10)							
Liquid Limit (%)		Undetermined					
Plasticity Index (%)		NP	≤ 12	✓			
Linear Shrinkage (%)		NP					
Material Strength - (SANS 3001 Method GR30,GR40 - SCALPED)							
MDD	Max Dry Density (kg/m ³)	1669					
	Optimum Moisture Content (%)	11.6					
	Mould Moisture Content (%)	11.8					
A	Relative Compaction (%)	100.0					
	Swell (%)	0.0	≤ 1.5	✓			
B	Relative Compaction (%)	95.6					
	Swell (%)	0.0					
C	Relative Compaction (%)	92.5					
	Swell (%)	0.0					
CBR	@100% Max Dry Density	12					
	@98% Max Dry Density	10					
	@95% Max Dry Density	9					
	@93% Max Dry Density	8	≥ 10	*			
	@90% Max Dry Density	6					
Material Condition							
Insitu Moisture Content (%)							
Soil Classification Achieved By The Material							
COLTO:		G8 SSG					
AASHTO System		A-3 / A-2-4					
Unified System		SW					

- Tests marked with a (*) are NOT SANAS Accredited results.
- Specimens delivered to Outeniqua Lab in good order.

Ruaan Lesch
Technical Signatory
For Outeniqua Lab (Pty) Ltd.

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Customer :	Outeniqua Geotechnical Services	Project :	Portion 91 of Matjiesfontein 304 - Keurboomstrand
	P O Box 964	Date Received :	08/02/2023
	Knysna	Date Reported :	22/02/2023
	6570	Req. Number :	0322/23
Attention :	Iain Paton	No. of Pages :	2/3

TEST REPORT CALIFORNIA BEARING RATIO

Sample Position (SV)		TP3	COLTO:			85882		
Depth (mm)		0-700	G9					
Sample No		85882	Subgrade					
Materials Description	Source	In-situ						
	Colour	Dark Grey						
	Soil Type	Silty Sand						
	Classification	Proposed (G9)						
Material Indicators - (SANS 3001 Method GR1)								
Percentage Passing	75 mm	100		Opinion				
	63 mm	100						
	50 mm	100						
	37.5 mm	100						
	28 mm	100						
	20 mm	100						
	14 mm	100						
	5 mm	100						
	2 mm	99						
	0.425 mm	94						
0.075 mm	7.4							
Material Indicators - (SANS 3001 Method PR5)								
Grading Modulus *		1.00	0.75 - 2.70	✓				
Coarse Sand Soil-Mortar (%)		6						
Atterberg Limits - (SANS 3001 Method GR10)								
Liquid Limit (%)		Undetermined						
Plasticity Index (%)		NP	≤ 12	✓				
Linear Shrinkage (%)		NP						
Material Strength - (SANS 3001 Method GR30,GR40 - SCALPED)								
MDD	Max Dry Density (kg/m ³)	1751						
	Optimum Moisture Content (%)	12.2						
	Mould Moisture Content (%)	12.1						
A	Relative Compaction (%)	100.0						
	Swell (%)	0.0	≤ 1.5	✓				
B	Relative Compaction (%)	95.8						
	Swell (%)	0.0						
C	Relative Compaction (%)	92.1						
	Swell (%)	0.0						
CBR	@100% Max Dry Density	20						
	@98% Max Dry Density	14						
	@95% Max Dry Density	8						
	@93% Max Dry Density	6	≥ 7	*				
	@90% Max Dry Density	3						
Material Condition								
Insitu Moisture Content (%)								
Soil Classification Achieved By The Material								
COLTO:		G9 Subgrade						
AASHTO System		A-3 / A-2-4						
Unified System		SP-SM						

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	P O Box 964	Date Received :	08/02/2023
	Knysna	Date Reported :	22/02/2023
	6570	Req. Number :	0322/23
Attention :	Iain Paton	No. of Pages :	3/3

TEST REPORT CALIFORNIA BEARING RATIO

Sample Position (SV)		TP4	COLTO:				
Depth (mm)		800-2600	G8 SSG				
Sample No		85883					
Materials Description	Source	In-situ					
	Colour	Light Yellow Orange					
	Soil Type	Sand					
	Classification	Proposed (G7)					
Material Indicators - (SANS 3001 Method GR1)							
Percentage Passing	75 mm	100		Opinion			
	63 mm	100					
	50 mm	100					
	37.5 mm	100					
	28 mm	100					
	20 mm	100					
	14 mm	100					
	5 mm	100					
	2 mm	100					
	0.425 mm	75					
0.075 mm	2.9						
Material Indicators - (SANS 3001 Method PR5)							
Grading Modulus *		1.22	0.75 - 2.70	✓			
Coarse Sand Soil-Mortar (%)		24					
Atterberg Limits - (SANS 3001 Method GR10)							
Liquid Limit (%)		Undetermined					
Plasticity Index (%)		NP	≤ 12	✓			
Linear Shrinkage (%)		NP					
Material Strength - (SANS 3001 Method GR30,GR40 - SCALPED)							
MDD	Max Dry Density (kg/m ³)	1614					
	Optimum Moisture Content (%)	11.2					
	Mould Moisture Content (%)	11.2					
A	Relative Compaction (%)	100.0					
	Swell (%)	0.0	≤ 1.5	✓			
B	Relative Compaction (%)	95.3					
	Swell (%)	0.0					
C	Relative Compaction (%)	92.8					
	Swell (%)	0.0					
CBR	@100% Max Dry Density	17					
	@98% Max Dry Density	14					
	@95% Max Dry Density	11					
	@93% Max Dry Density	9	≥ 10	*			
	@90% Max Dry Density	7					
Material Condition							
Insitu Moisture Content (%)							
Soil Classification Achieved By The Material							
COLTO:		G8 SSG					
AASHTO System		A-3 / A-2-4					
Unified System		SP					

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For Outeniqua Lab (Pty) Ltd.

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Appendix 4

DCP test data



Geotechnical Engineering Consultants

Registration No. 1999/062743/23

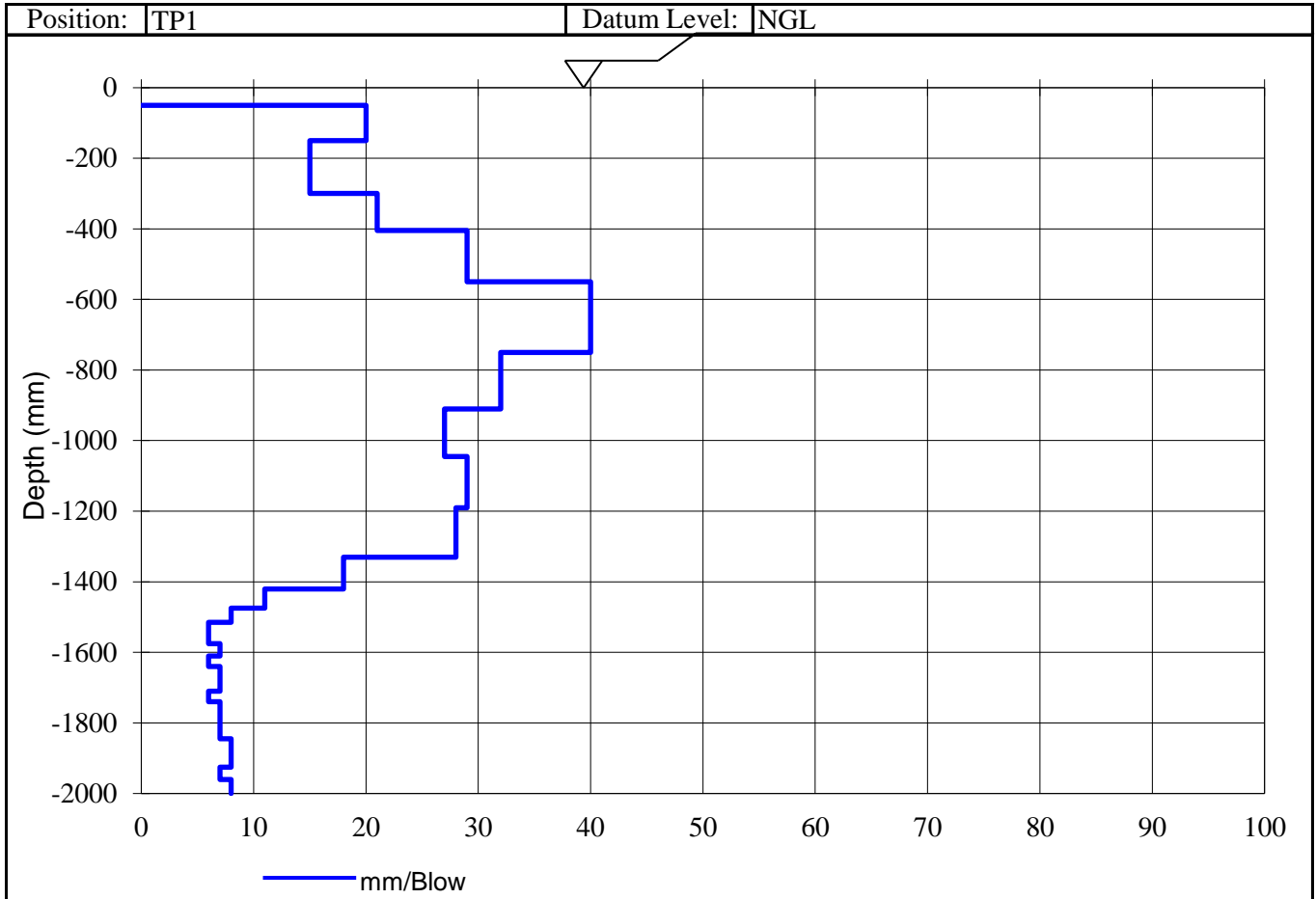
18 Clyde Street, Knysna : PO Box 964, Knysna, 6570

Tel: 044 3820502 : Fax: 044 3820503 : e-mail: iain@outeniqualab.co.za

Customer :	Poise Consulting Engineers	Project :	Portion 91 of Matjiesfontein 304 Keurboomstrand
	P.O. Box 1018	Date Received :	24.01.2023
	Plettenberg Bay	Date Reported :	01.02.2023
	6600	Req. Number :	
Attention :	Deon Botes	No. of Pages :	1 of 10

TEST REPORT

Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



I Paton (Member)
For Outeniqua Geotech. Services cc.
Technical Signatory

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Geotechnical Engineering Consultants

Registration No. 1999/062743/23

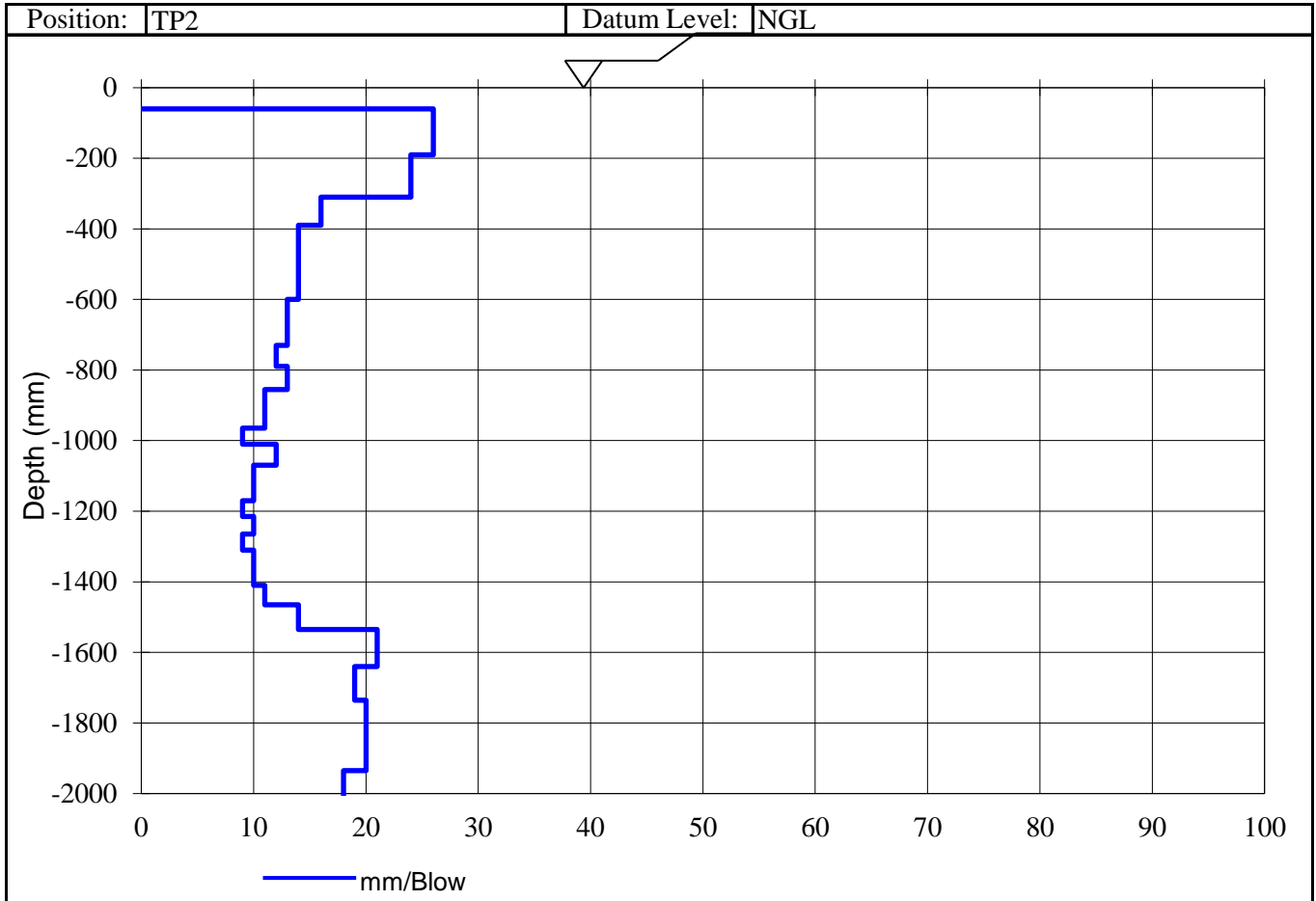
18 Clyde Street, Knysna : PO Box 964, Knysna, 6570

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	Plettenberg Bay	Date Reported :	01.02.2023
	6600	Req. Number :	
Attention :	Deon Botes	No. of Pages :	2 of 10

TEST REPORT

Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



I Paton (Member)
For Outeniqua Geotech. Services cc.
Technical Signatory

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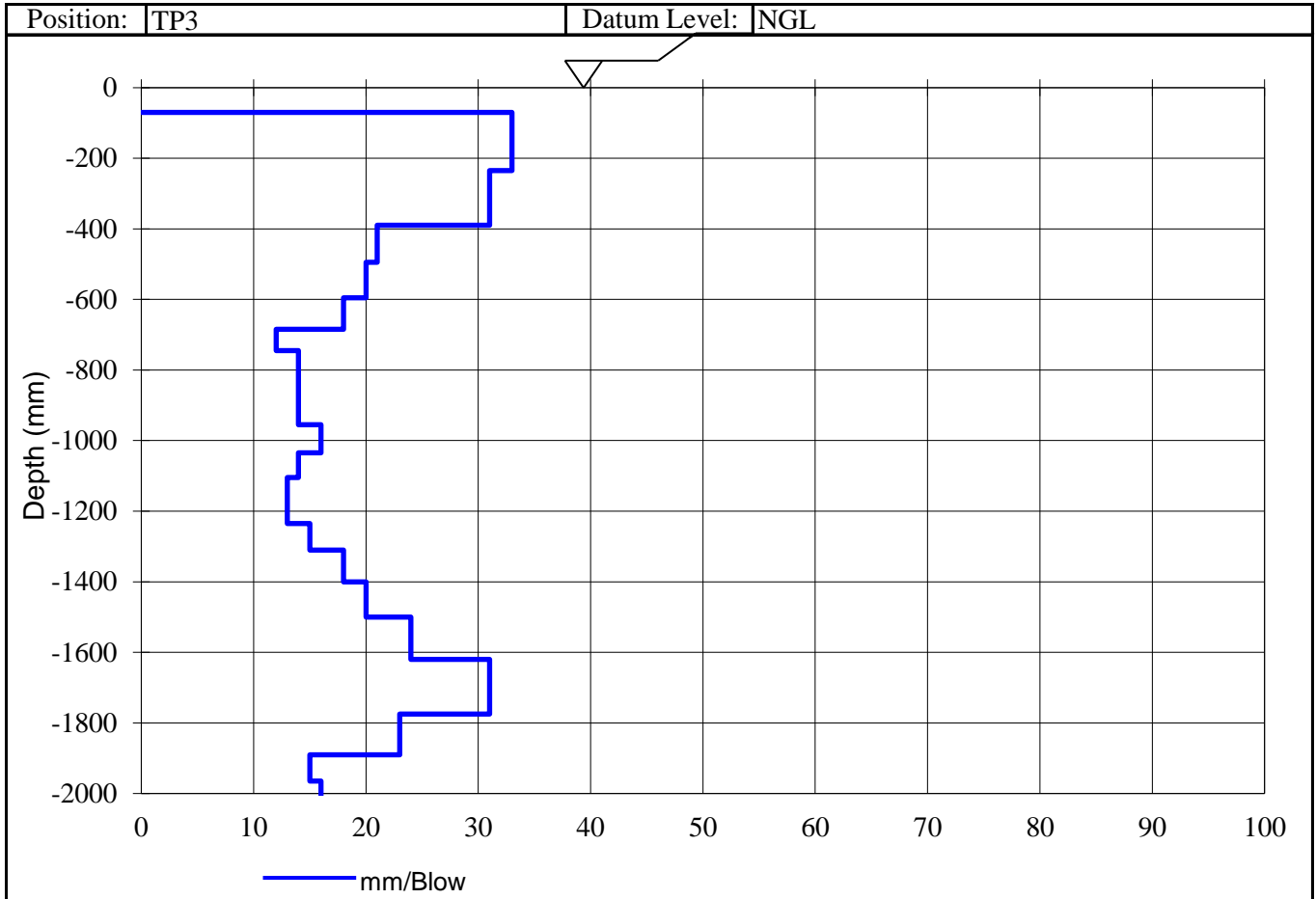
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R-DCP-1-5

Dec-14

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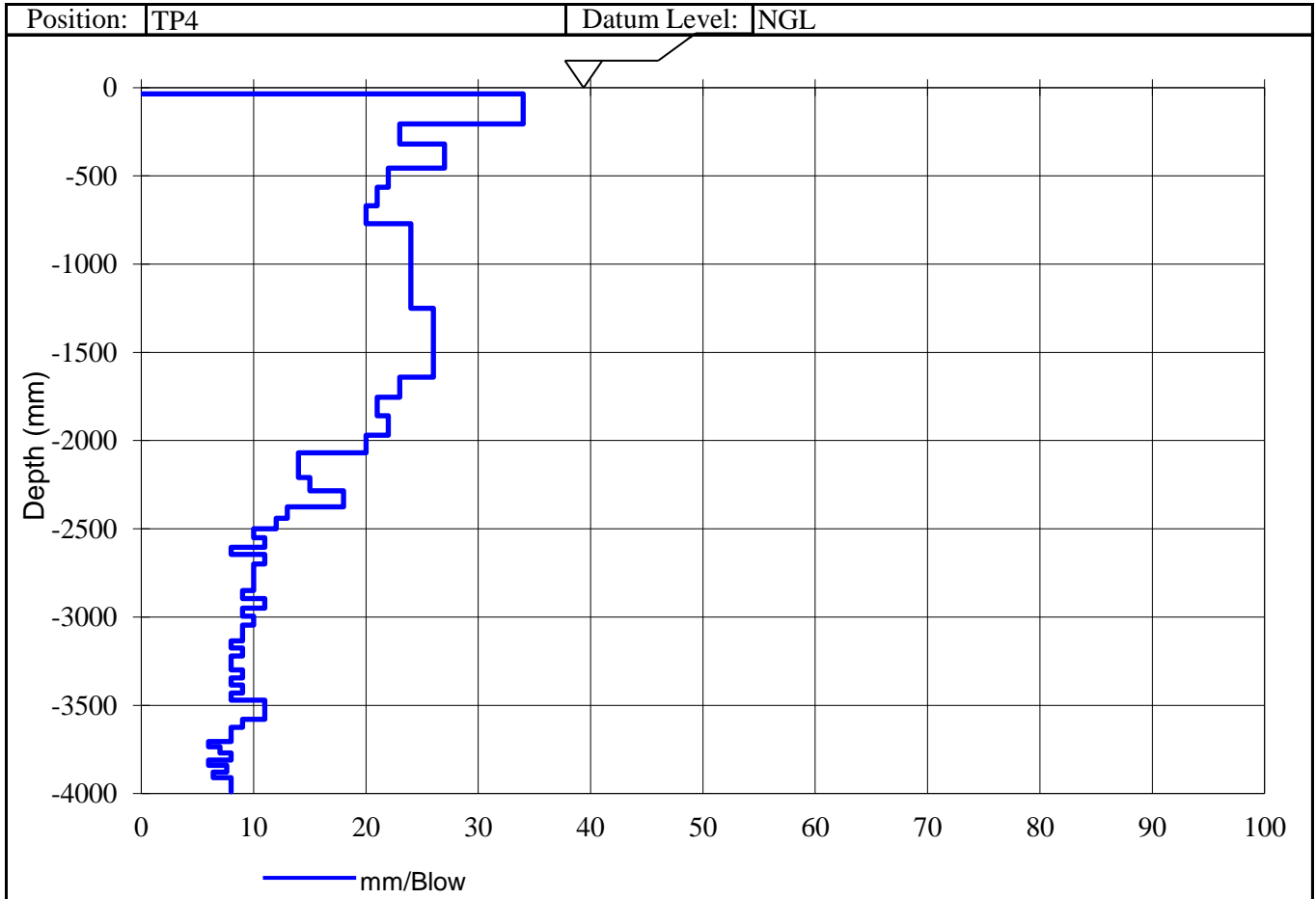
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Members: Iain Paton BSc Hons MEng Pr Sci Nat MSAIEG MSAICE



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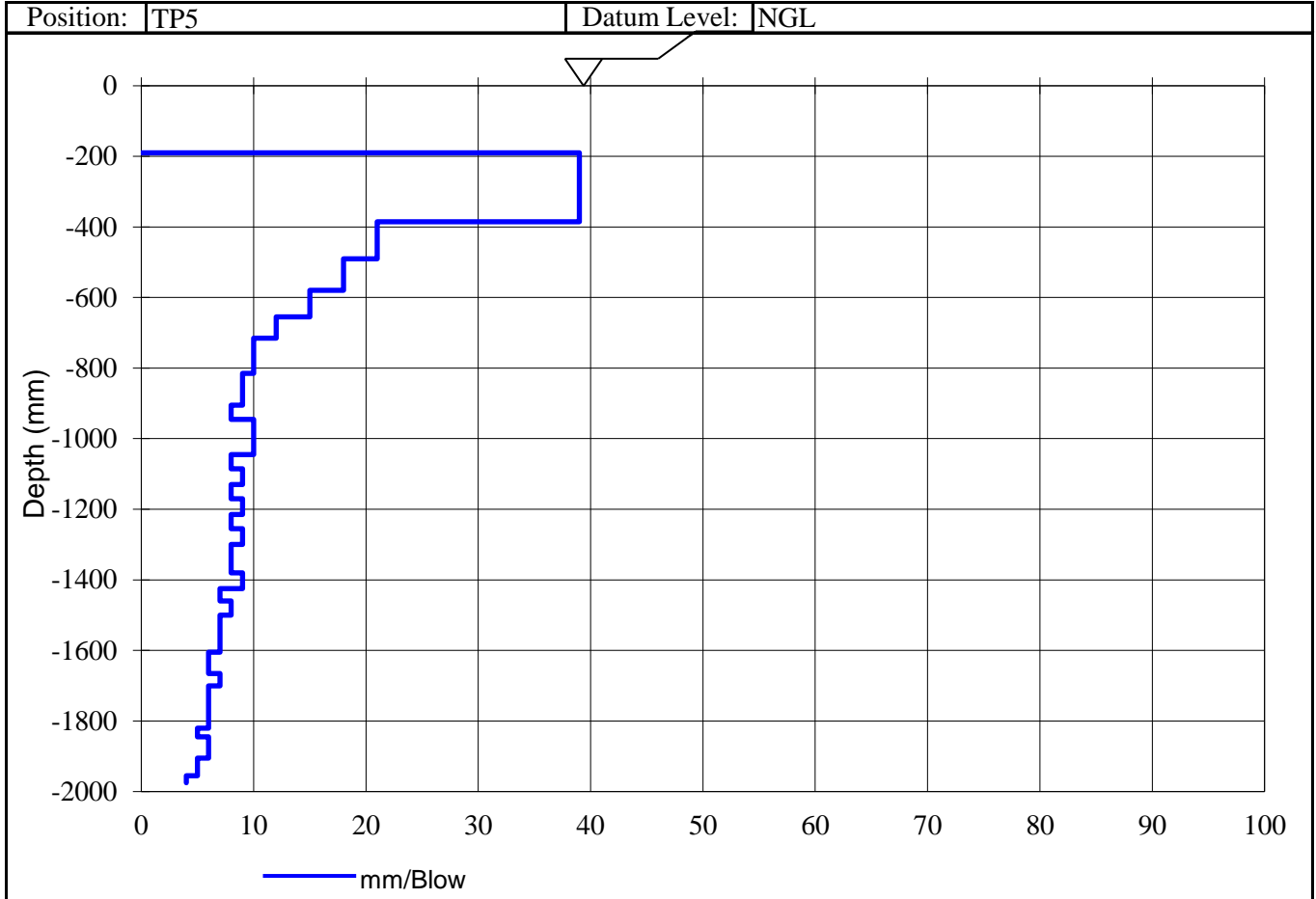
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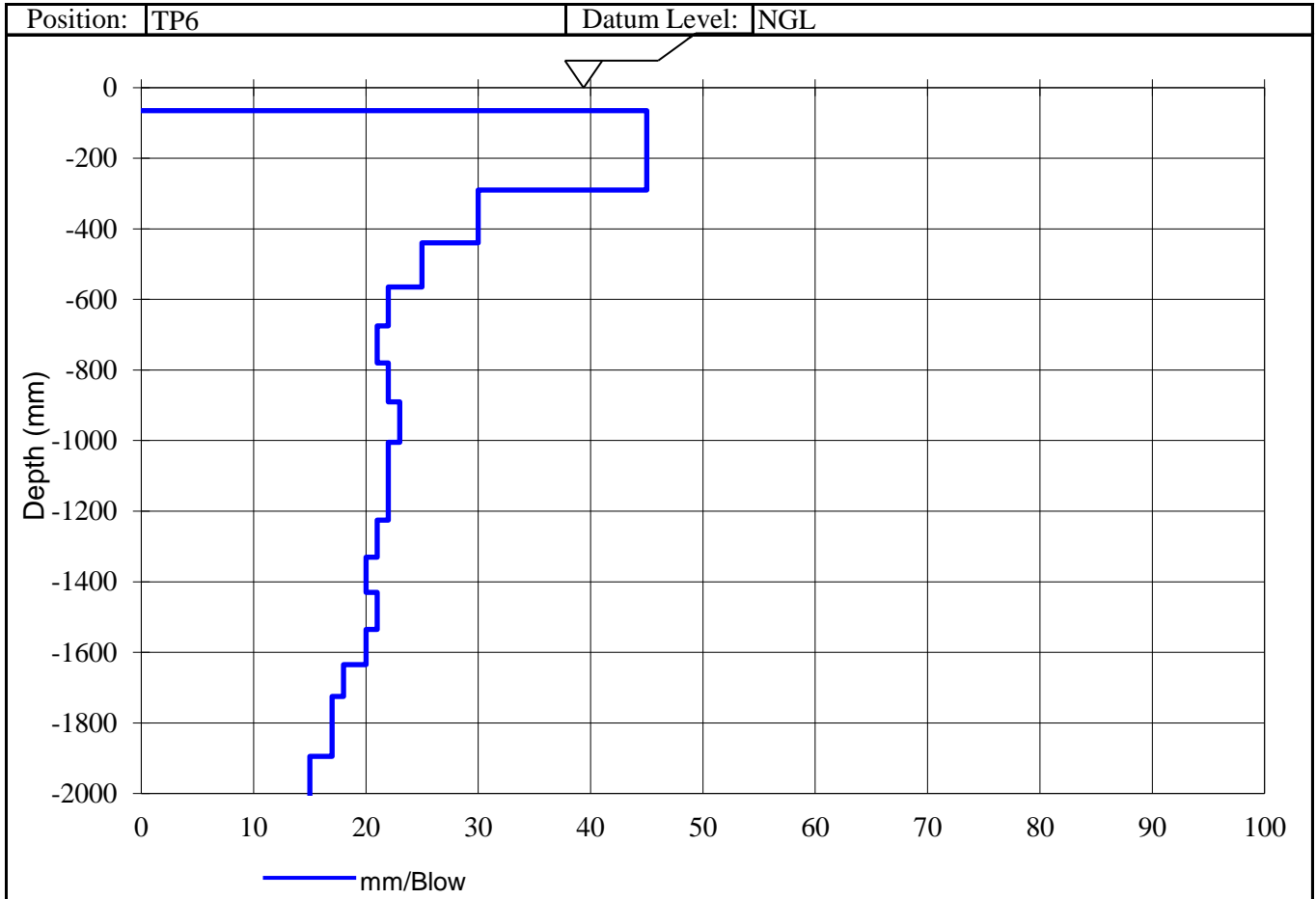
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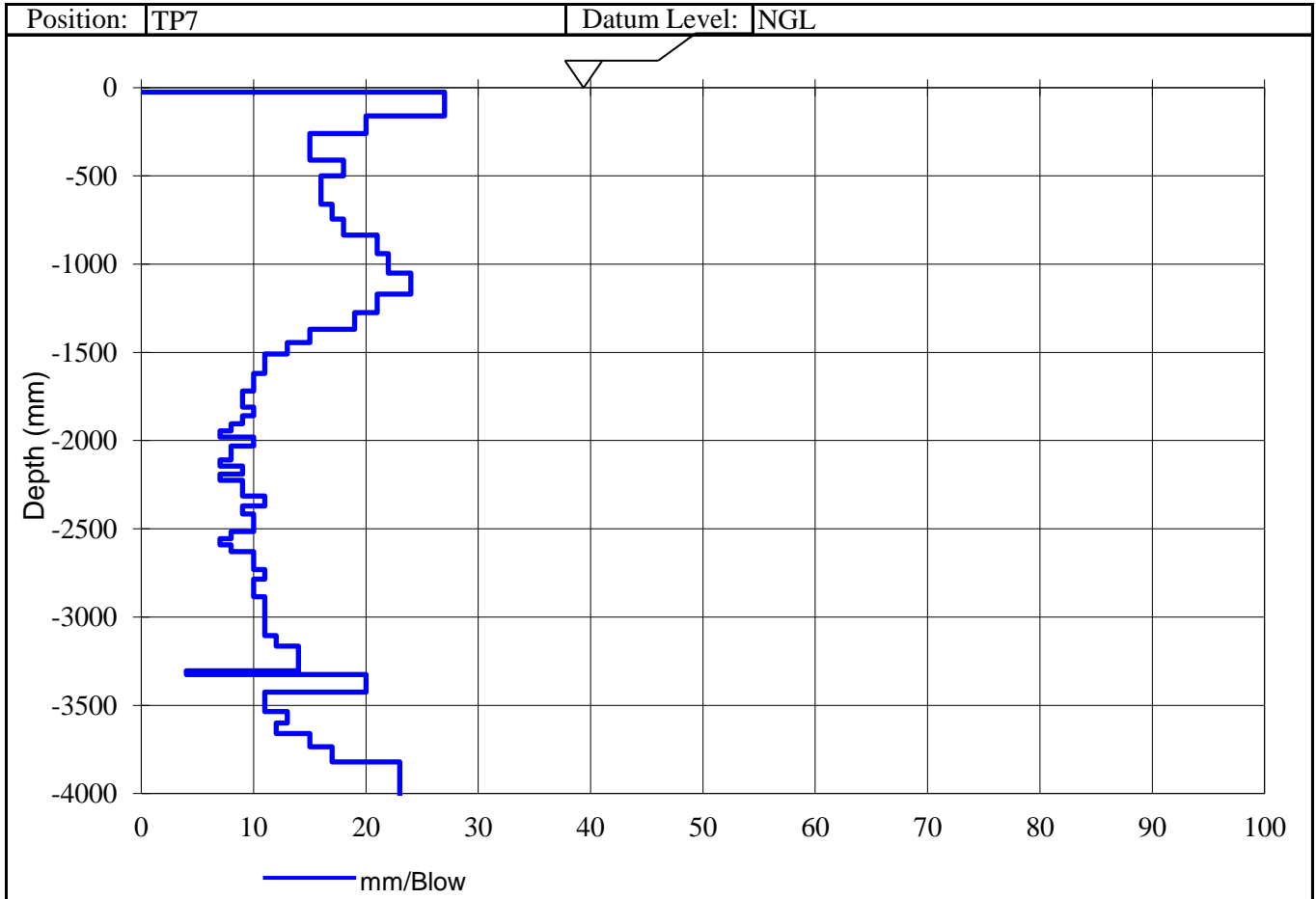
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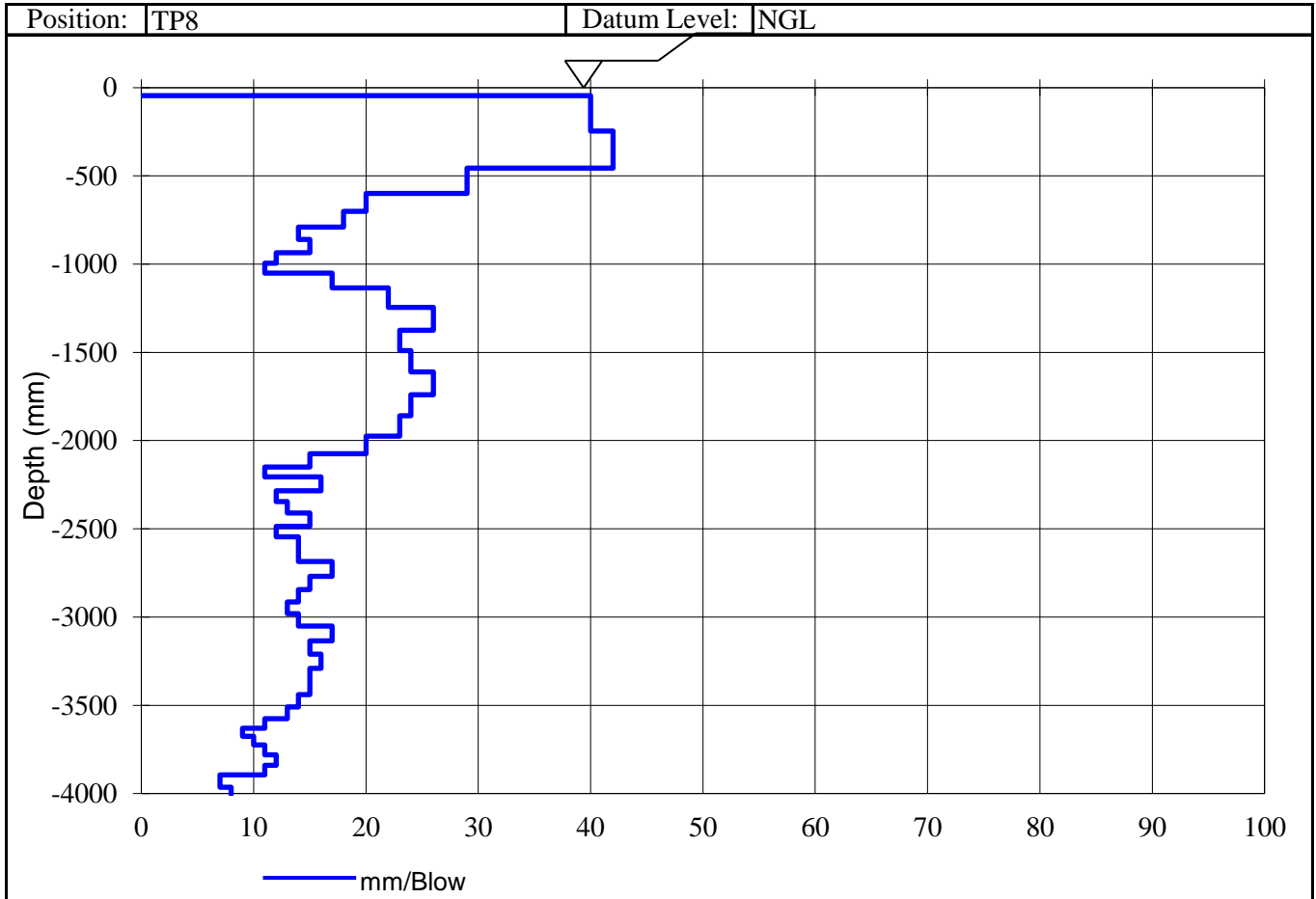
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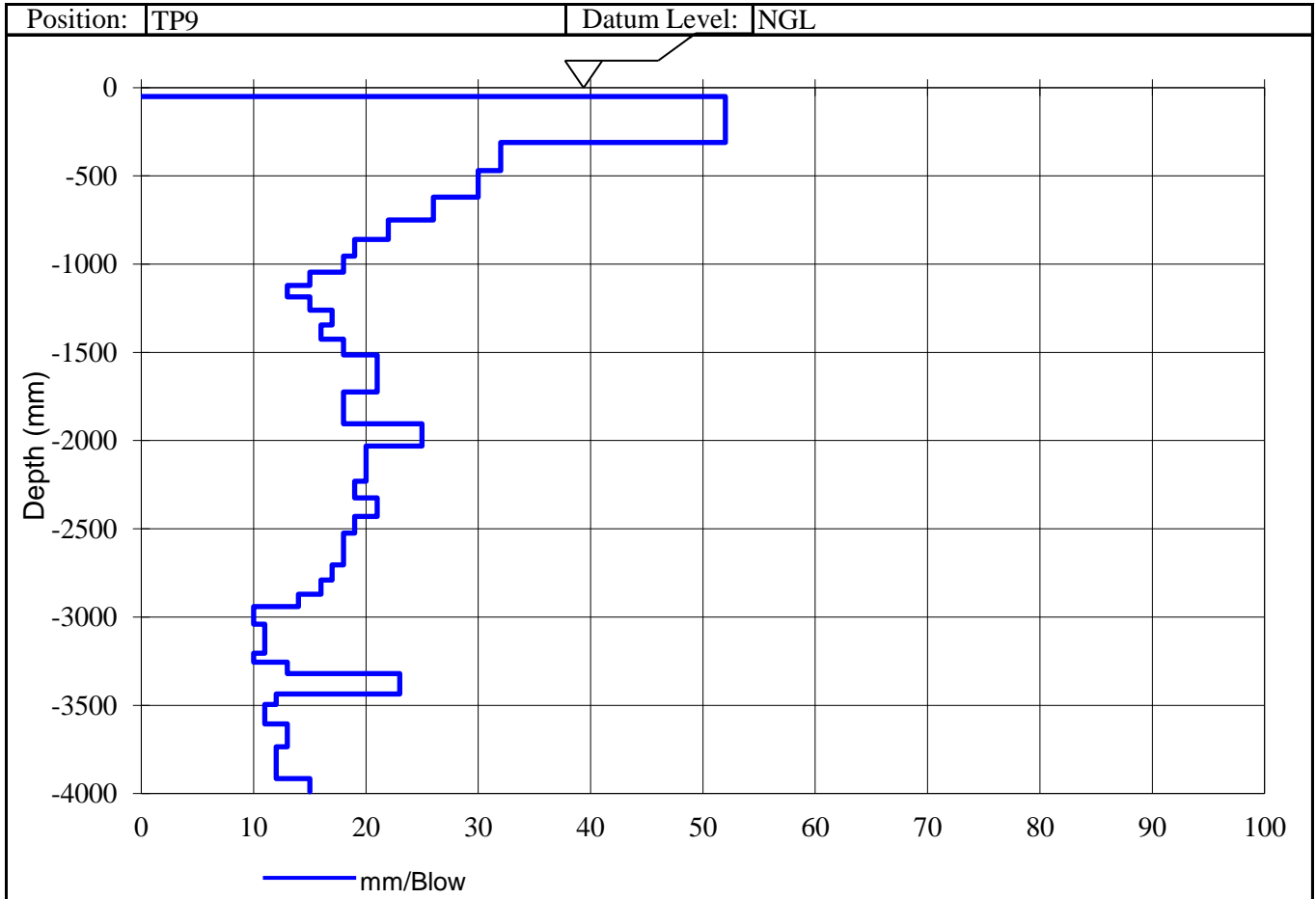
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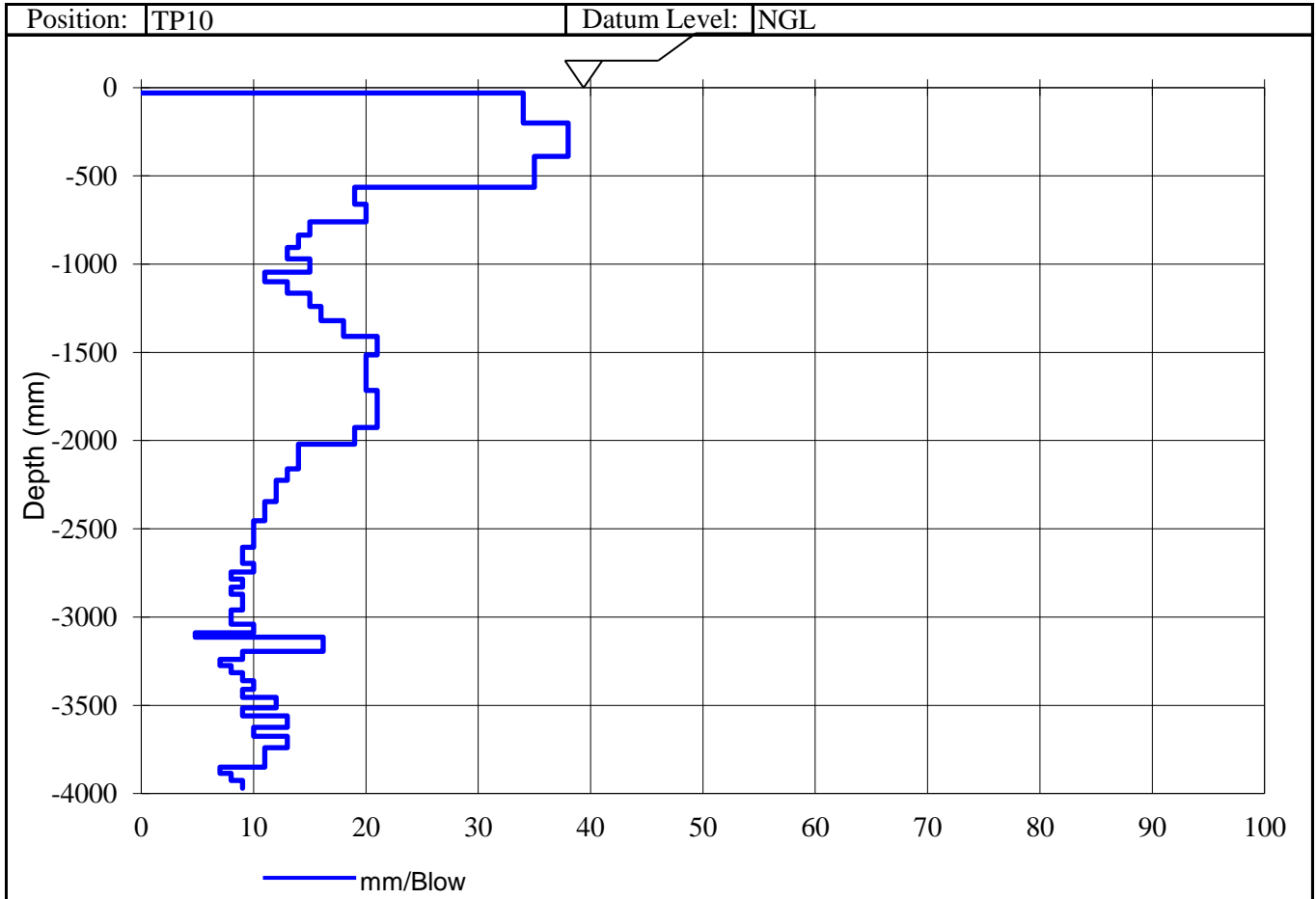
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