

GEOTECHNICAL SOIL TEST REPORT

Client: Mr Coetzee

Project: Erf 2003, Wilderness

Date of test: 23.7.2021

Geotechnical Constraint	Risk			NHBC Classification
	Low	Medium	High	
Active clay	X			H
Compressible soil		X		
Collapsible soil		X		C1
Imported/uncontrolled fill	X			
Chemically aggressive soils	X			
Saturated soils/ groundwater seepage		X		
Shallow hard rock/ difficult excavations		X		R
Slope stability problems	X			
Flood potential	X			
Seismicity	X			
Dolomitic land	X			

Disclaimer: The above classification is provided as a guideline and is true for the specific locations that were tested and may not be true for the entire site.

Site description:

The topography of the property is quite variable and is characterised by a south- and southeast-facing moderate slope which becomes steeper towards a natural drainage line in the middle of the property. The proposed development consists of 4 chalets and a main residence along the northern and north-eastern side of the site. At the time of the investigation, the site was covered in thick indigenous vegetation and entry onto the site was restricted to access on foot (see Figure 1). The ground surface conditions in the proposed development area were generally dry with no signs of groundwater seepage or any significant slope stability problems.



Figure 1: View of site from the access point on the NE corner

Geology & Soil profile:

The site is underlain by phyllite, schist and feldspathic quartzite of the Soetkraal Formation of the Kaaimans Group. The geology is not visible in outcrop on the site, but this formation is well exposed on Whites Road to the east of the site and on the Kaaimans pass between Wilderness and George. The Kaaimans Formation rocks in the area were intruded by the George granite pluton and are generally southward-dipping at angles varying from 40-70°.

The soil profile that underlies the site was investigated by way of four shallow test pits, and found to consist of the following general horizons:

0-0.3m: Dark brown, firm, gravelly sandy clay/clayey sand – ***colluvium (topsoil)***

0.3-0.8m: Dark reddish brown, stiff, shattered, sandy silty clay - ***colluvium***

0.8-1.0m: Light grey to dark brown, dense to very dense, silty clayey gravel - ***residual completely weathered phyllite***

>1.0m: Light grey, very highly fractured, highly weathered, very soft to soft rock – ***phyllite bedrock***

The test pits were terminated due to difficult excavations or refusal on phyllite bedrock (see Fig 2). The depth to the bedrock is variable, and becomes shallower towards the west, but generally occurs at a depth of 0.8-1.5m. Large boulders or fragments of bedrock may also be encountered at this depth. No groundwater was encountered in test pits, but seepage can be expected in wet weather periods.

Observations in test pits and subsequent lab tests indicates a slightly expansive nature of the clayey soil cover above the bedrock, but this horizon is generally limited in thickness and the overall heave potential of the site is low.

In situ DCP tests conducted next to test pits from NGL indicate that the upper ~0.4m of the soil profile is loose, but firms up quickly below this depth and most tests refused on rock or boulders at a max depth of 1.5m. The DCP at TP1 penetrated in stiff material to 2m depth, indicating deeper rock at this position.

The founding conditions appear to be favourable with good bearing capacity on stiff/dense soil or rock at fairly shallow founding depths of 0.8m where EASBP ~ 125kPa, but variable rock levels may have an influence on final foundation levels.



Figure 3: Soil types encountered in test pits

Recommendations:

Earthworks & materials: The site is moderately sloping, becoming steep towards the west, and access/vegetation clearing will be challenging unless a minimal footprint area is adopted. Earthworks required to create level platforms (if any) may encounter shallow rock, mainly on the western side of the proposed development. Shallow excavations for the proposed development are unlikely to have any significant effect on the general stability of the site, but excavations should be assessed by a competent person as excavations progress. Excavations shallower than 1.5m are likely to be fairly stable at near-vertical angles for short periods (temporary works).

In situ granular soils (sandy/gravelly soils, not clay), less any large rock fragments >150mm diameter, obtained from excavations may be suitable for reuse as bulk filling material under floors and behind retaining walls but should be approved by the engineer before placement. Any unsuitable soil obtained from excavations should be spoiled in a suitable location on site (e.g. as landscaping fill). Allowance should be made for imported high quality materials (e.g. G5) for final selected fill layers under concrete surface beds. Imported free-draining fill material (coarse sand/crusher run/stone) will be required for drainage medium behind retaining walls (if any).

Foundations & floors: The recommended foundation type for single or double storey masonry or timber structures is reinforced strip and/or pad foundations placed on dense/stiff soil horizons or preferably bedrock at a minimum nominal depth of 0.8m below NGL. The recommended maximum bearing pressure for foundations is 125kPa. Structures founded at the correct levels on suitable bedrock or stiff/dense soil horizons are unlikely to induce or become susceptible to slope instability. Competent supervision in this regard is important. All foundations should be inspected by the engineer before placing reinforcement.

Driveway & parking areas: The proposed driveway onto the site with parking area will be a challenge due to the dense indigenous vegetation, which may be environmentally sensitive. Construction of the driveway may involve minor cutting and filling to achieve the correct line and levels. The in situ soils are generally poor quality in terms of road-building and it is recommended that an allowance is made for the importation of SSG gravel material to improve access during construction, in addition to the final subbase and paving layerworks.

Drainage: The soil has a low permeability and vertical infiltration will be restricted by the presence of shallow rock and dense soils, so stormwater will tend to run off site after heavy rainfall. Effective stormwater management systems are required to collect and discharge stormwater in a controlled manner down slopes. Subsoil drains are recommended behind retaining walls as standard.

Conclusions:

The investigation indicates that the site is potentially suitable for development but there are some geotechnical constraints, such as difficult access, restricted construction space, steep slopes and shallow/irregular rock, which may have an impact on the engineering design and construction costs. Some recommendations are offered for consideration by the structural engineer.

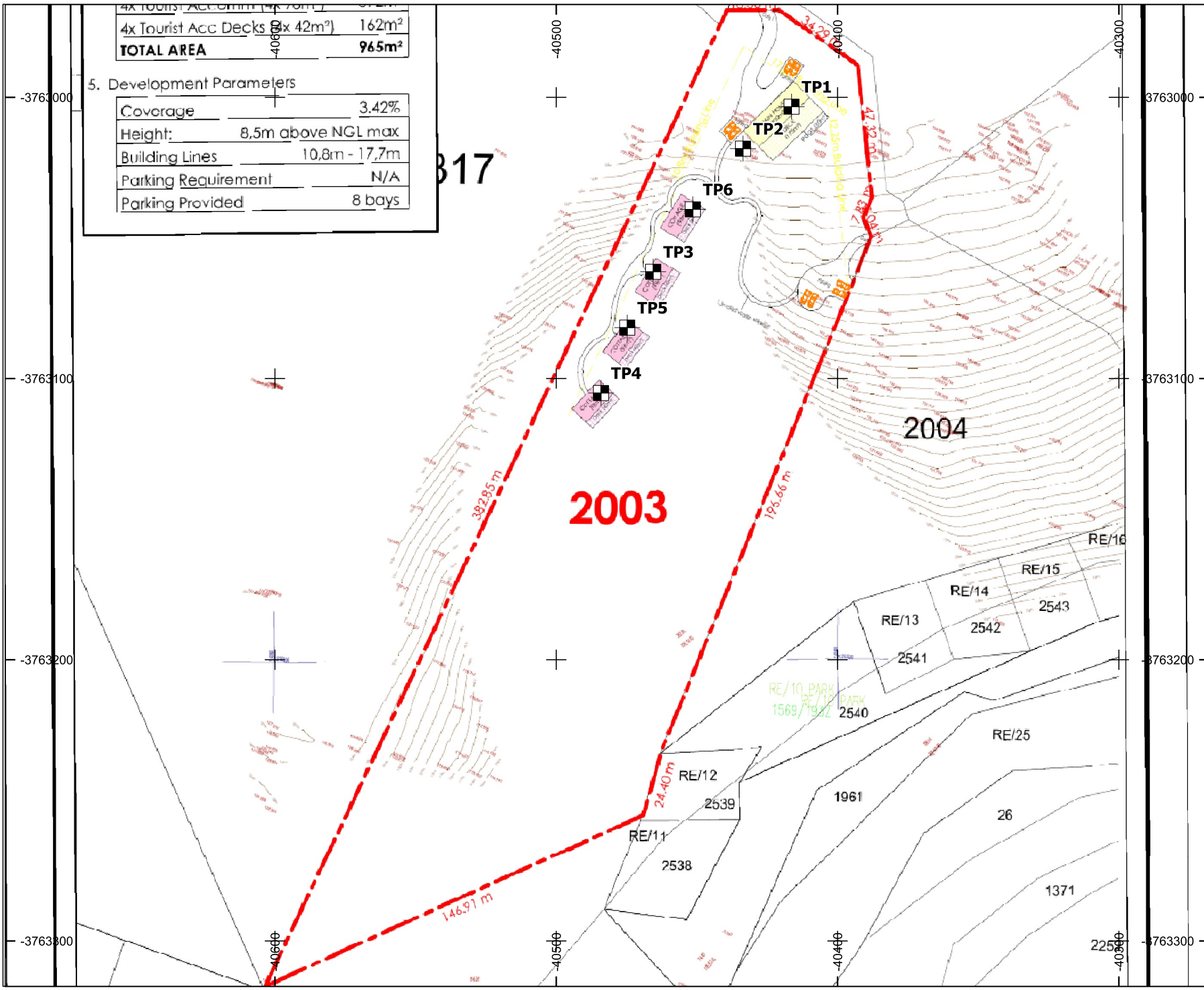
A handwritten signature in black ink, appearing to read 'Iain Paton', written in a cursive style.

Iain Paton Pr Sci Nat Pr Tech Eng

4x Tourist Acc Decks (42m ²)	162m ²
TOTAL AREA	965m²

5. Development Parameters

Coverage	3,42%
Height:	8,5m above NGL max
Building Lines	10,8m - 17,7m
Parking Requirement	N/A
Parking Provided	8 bays



Legend

Test pit/ DCP test position

Client: Wentzel Coetzee
 Project: Residential Development
 Site: Erf 2003 Wilderness Area: George

Drawing Name: Geotechnical Plan (2)
 Drawing No:
 Date: August 2021
 Revision: 0
 Drawn by: DB Snyders
 Checked by: I Paton





Scale: 1:1 800



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Legend

-  Test pit/ DCP test position
-  Farm Portions
-  Erf
-  Contours 5m

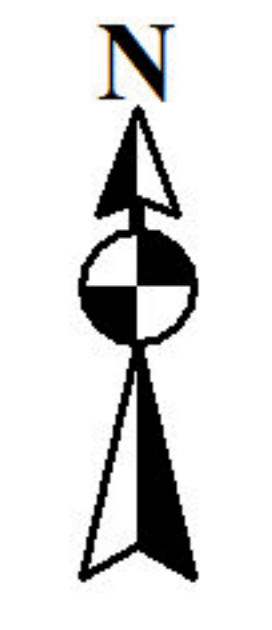
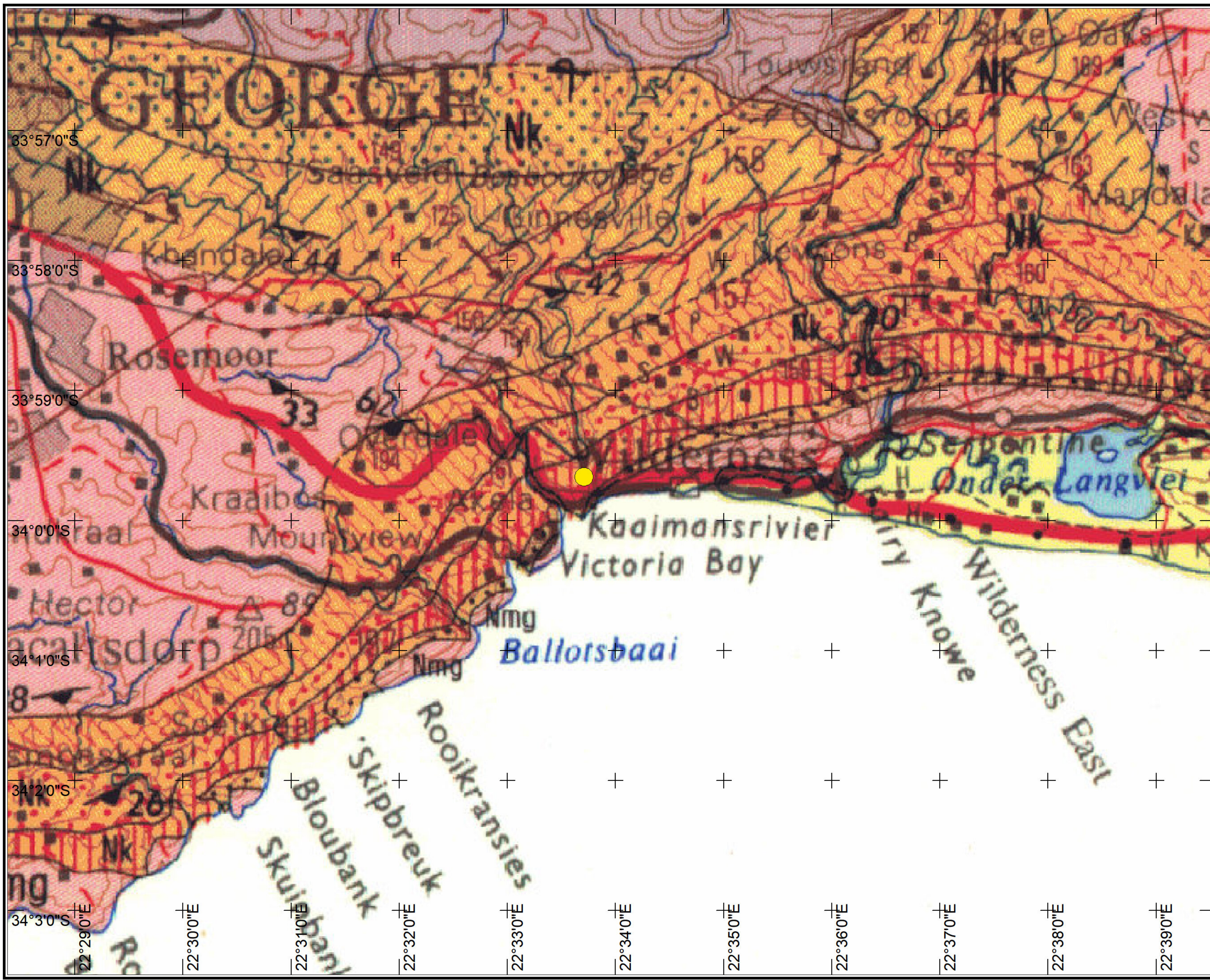
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 Project: Residential Development
 Site: Erf 2003 Wilderness Area: George

Drawing Name: Geotechnical Plan
 Drawing No:
 Date: August 2021
 Revision: 0
 Drawn by: DB Snyders
 Checked by: I Paton

Scale: 1:1 800

 10 0 10 20 30 40 m



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Legend

● Site locality

Client: Mr Coetzee
 Project: New development
 Site: Erf 2003
 Area: Wilderness

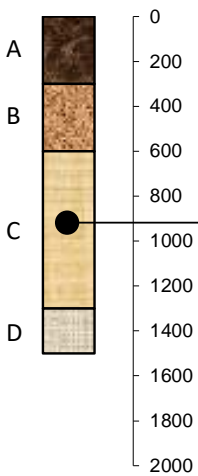
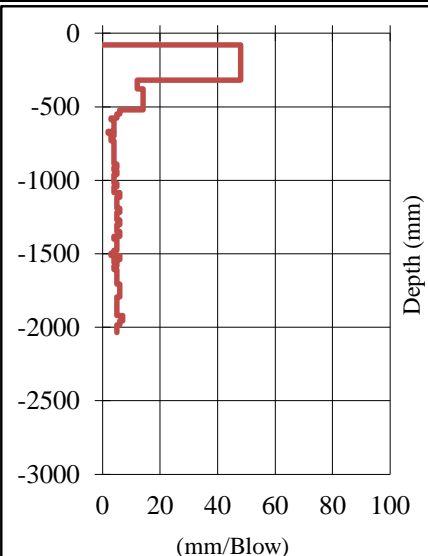
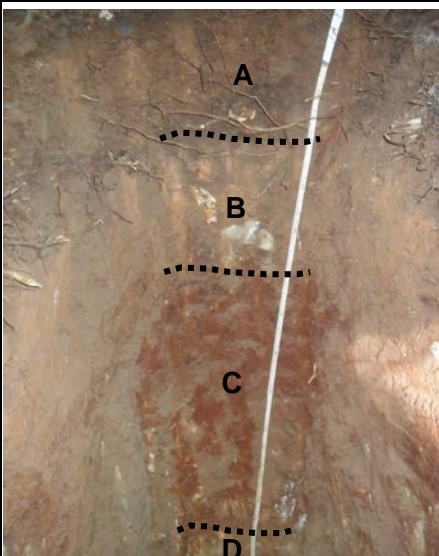
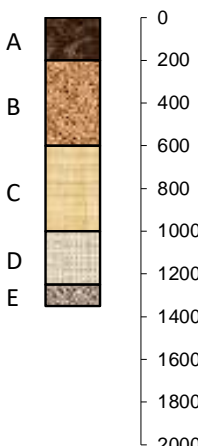
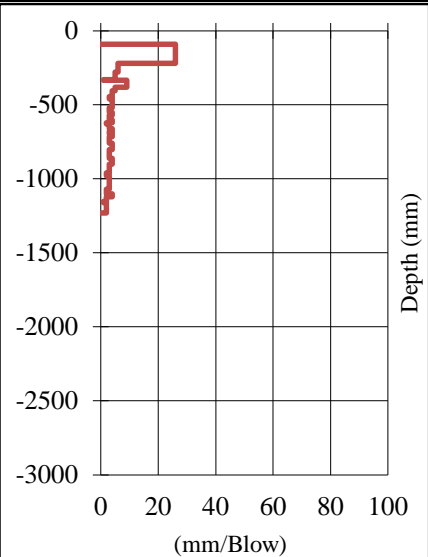
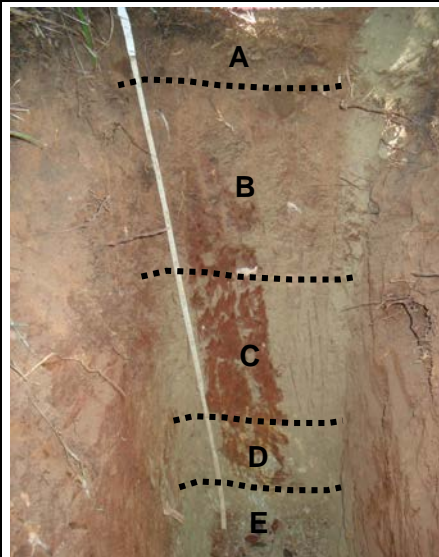
Drawing Name: Geology
 Drawing No:
 Date: July 2021
 Revision: 0
 Drawn By: S Ngema
 Checked By: I Paton



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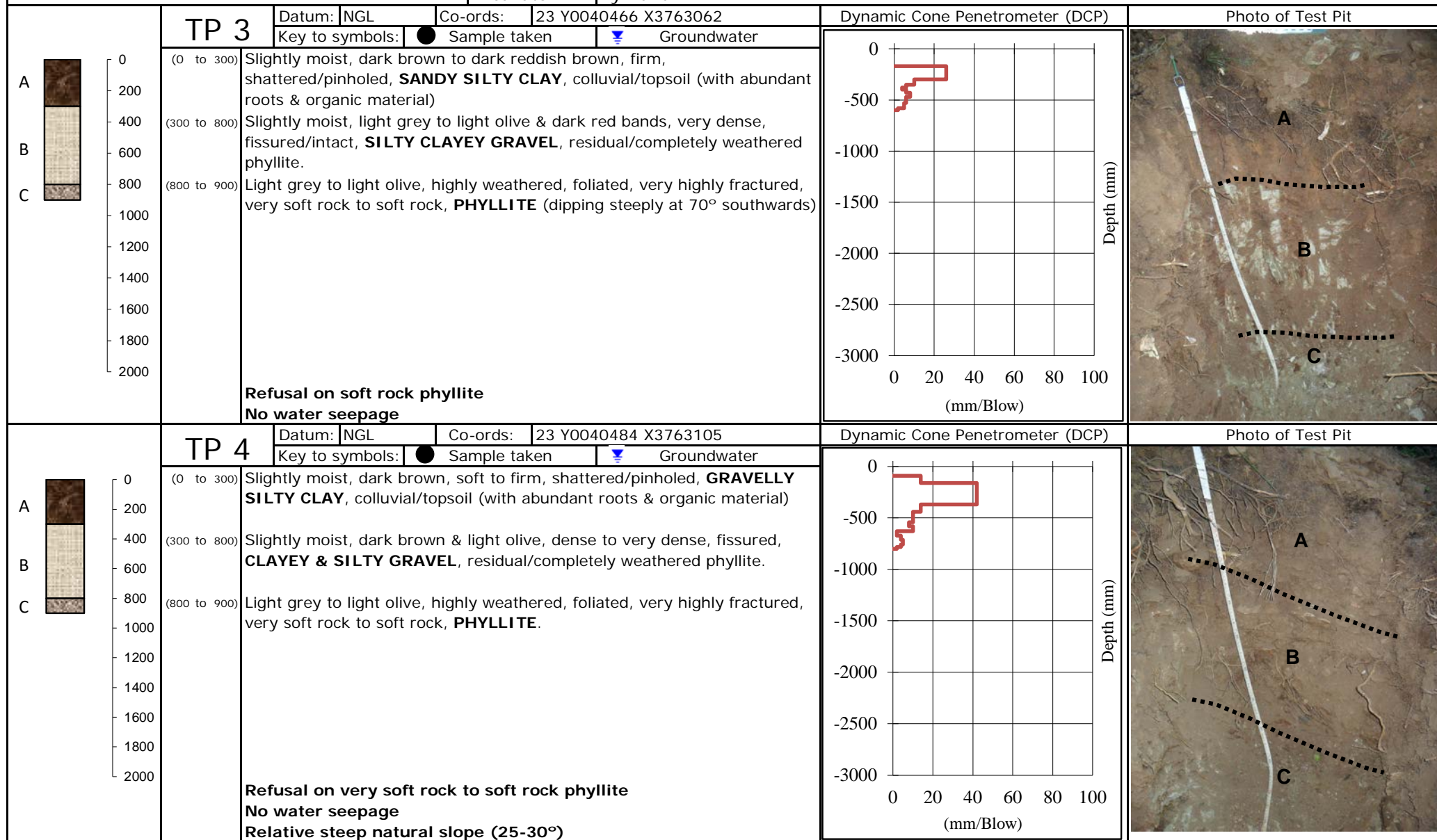
Geotechnical Soil Profile

Client: Wentzel Coetzee
 Project: Erf 2003 Wilderness
 Area: George
 Date: 23.07.2021
 Excavator: By Hand

		Datum: NGL	Co-ords: 23 Y0040416 X3763003	Dynamic Cone Penetrometer (DCP)	Photo of Test Pit
 <p>A 0 200 B 400 600 C 800 1000 1200 D 1400 1600 1800 2000</p>	TP 1	Key to symbols: ● Sample taken	☒ Groundwater	 <p>Depth (mm) 0 -500 -1000 -1500 -2000 -2500 -3000 (mm/Blow) 0 20 40 60 80 100</p>	 <p>A B C D</p>
	(0 to 300) Slightly moist, dark brown to dark reddish brown, firm, shattered/pinholed, SANDY SILT & CLAY , colluvial/topsoil (with abundant roots & organic material) (300 to 600) Slightly moist, dark reddish brown, stiff, micro-shattered, SANDY SILTY CLAY , colluvial (with traces of fine to coarse gravel) (600 to 1300) Slightly moist, dark red, stiff to very stiff, micro-shattered, SLIGHTLY SANDY SILTY CLAY , colluvial (with traces of fine to coarse gravel) (1300 to 1500) Slightly moist, dark reddish & yellowish orange, very stiff, intact/fissured, SILTY CLAY , residual phyllite (with some fragments of very soft rock phyllite) TP stopped No water seepage				
 <p>A 0 200 B 400 600 C 800 D 1000 E 1200 1400 1600 1800 2000</p>	TP 2	Key to symbols: ● Sample taken	☒ Groundwater	 <p>Depth (mm) 0 -500 -1000 -1500 -2000 -2500 -3000 (mm/Blow) 0 20 40 60 80 100</p>	 <p>A B C D E</p>
	(0 to 200) Slightly moist, dark brown to dark reddish brown, firm, shattered/pinholed, SANDY SILTY CLAY , colluvial/topsoil (with abundant roots & organic material) (200 to 600) Slightly moist, dark reddish brown, stiff, micro-shattered, SANDY SILTY CLAY , colluvial (with some roots & traces of gravel) (600 to 1000) Slightly moist, dark red, very stiff, shattered/micro-shattered, SANDY SILTY CLAY , colluvial (with scattered weathered gravel) (1000 to 1250) Slightly moist, dark reddish & yellowish orange, very stiff to hard, shattered/fissured, GRAVELLY SILTY CLAY , residual (with some very soft rock to soft rock remnants) (1250 to 1350) Light brown to light olive, highly weathered to completely weathered, foliated, very highly fractured, very soft to soft rock PHYLLITE . Near refusal on very soft to soft rock No water seepage				

Geotechnical Soil Profile

Client:	Wentzel Coetzee
Project:	Erf 2003 Wilderness
Area:	George
Date:	23.07.2021
Excavator:	By Hand





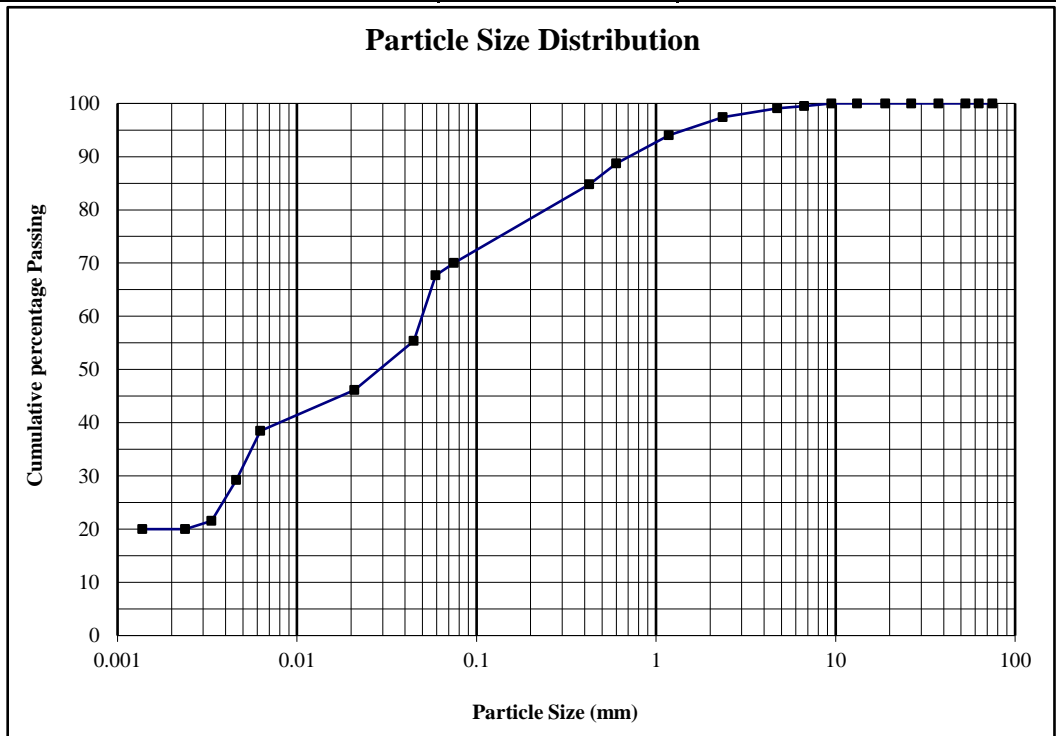
Customer :	Outeniqua Geotechnical Services	Project :	Erf 2003 - Wilderness
	P O Box 964	Date Received :	26/07/21
	Knysna	Date Reported :	30/07/21
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	Iain Paton	No. of Pages :	1

TEST REPORT

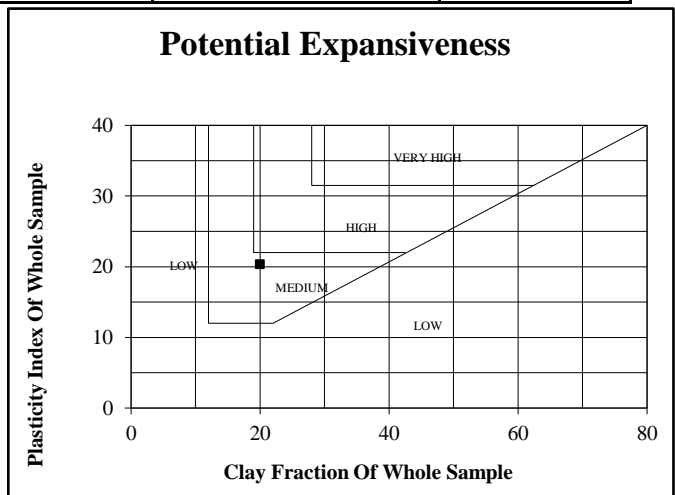
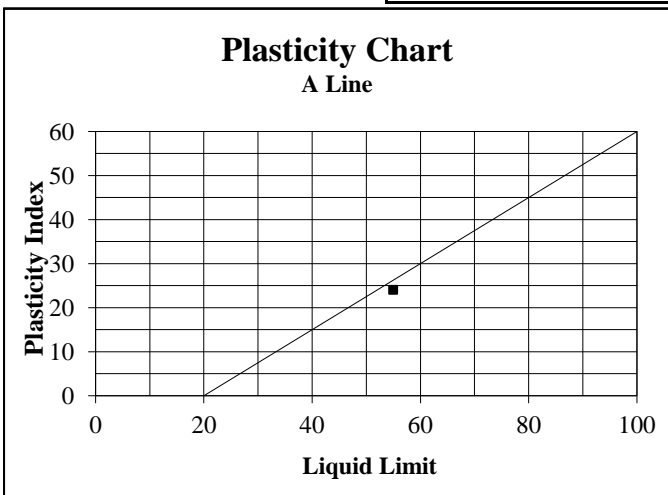
FOUNDATION INDICATOR - (TMH 1 Method A1(a),A2,A3,A4,A5) & (ASTM Method D422)

Material Description:	Dark Red Clayey Sandy Silt	Sample Number:	81971		
Position:	TP1 - Layer 2	Liquid Limit	55	Linear Shrinkage	12
Depth:	600-1300	Plasticity Index	24	Insitu M/C%	22

Sieve Size(mm)	% Passing
75.0	100
63.0	100
53.0	100
37.5	100
26.5	100
19.0	100
13.2	100
9.5	100
6.7	100
4.75	99
2.36	97
1.18	94
0.600	89
0.425	85
0.075	70
0.0591	68
0.0447	55
0.0209	46
0.0062	38
0.0046	29
0.0033	22
0.0024	20
0.0014	20



% Clay	20	% Silt	48	% Sand	28	% Gravel	4
Unified Soil Classification		MH		PRA Soil Classification		A-7-5	



Notes:

- Specimens delivered to Outeniqua Lab in good order.

1. Sampling falls outside the scope of Outeniqua Lab's SANAS accreditation.

For Outeniqua Lab (Pty) Ltd.

2. The test results are reported with an approximate 95% level of confidence.

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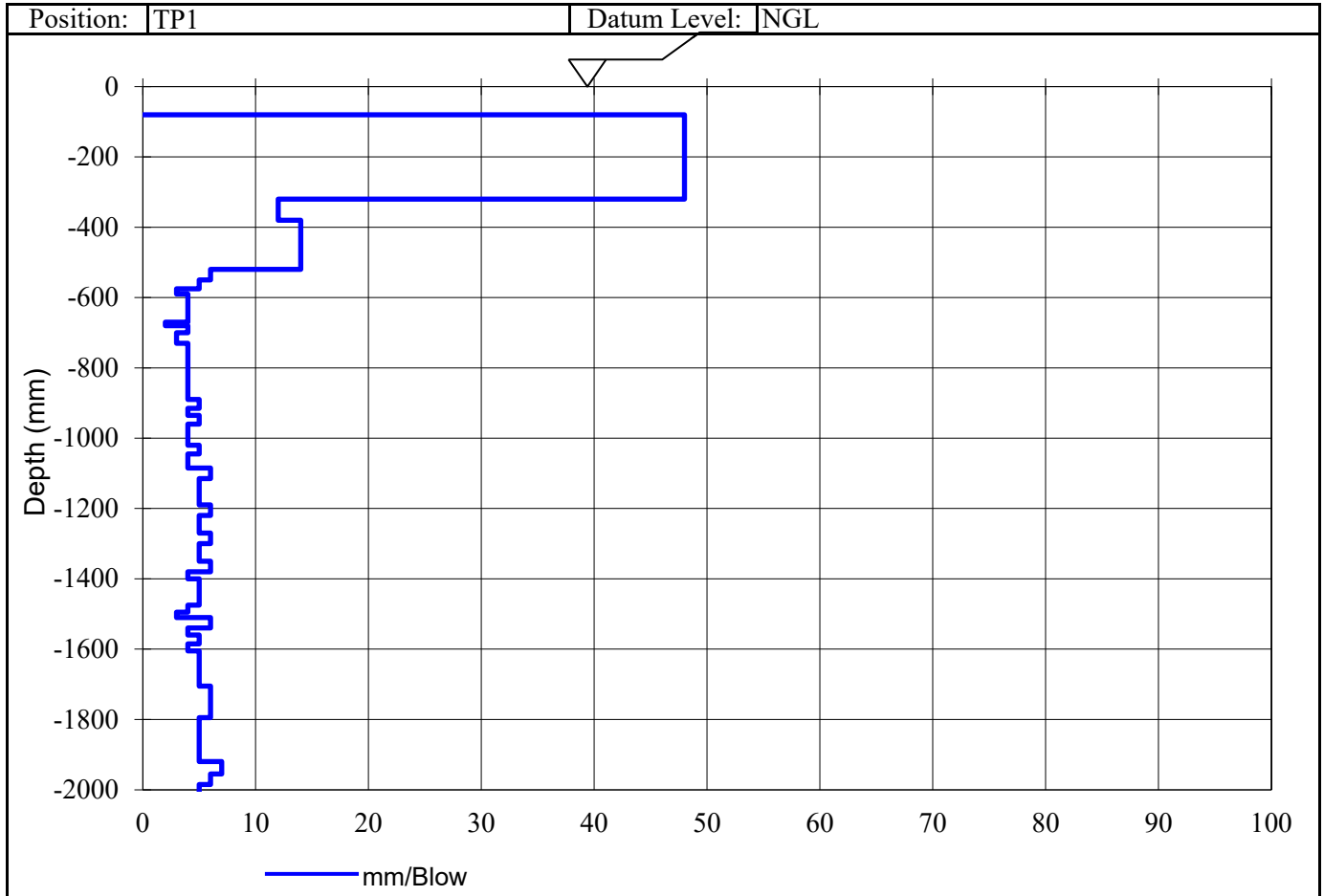
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		Req. Number :	
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TEST REPORT

Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



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Technical Signatory

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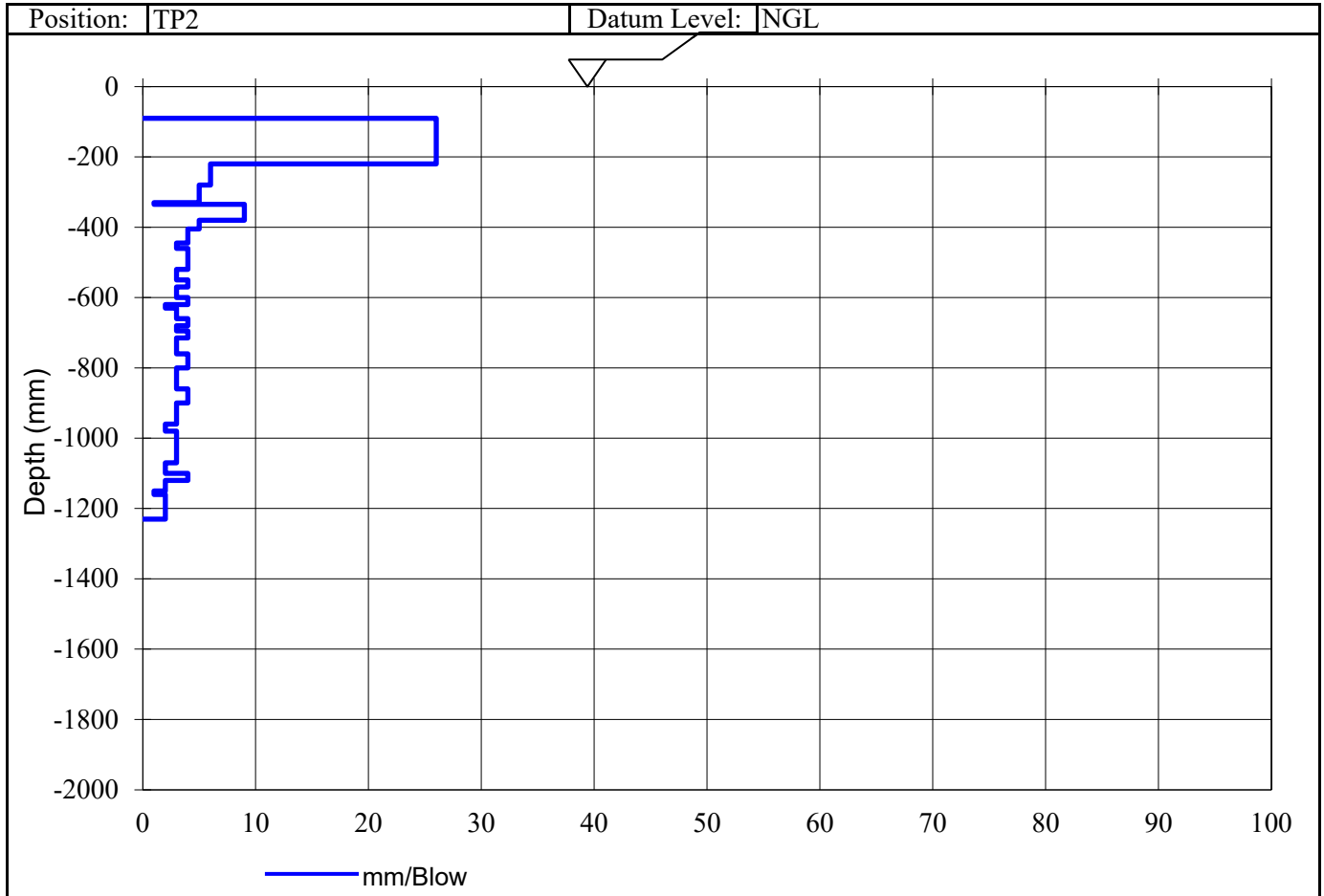
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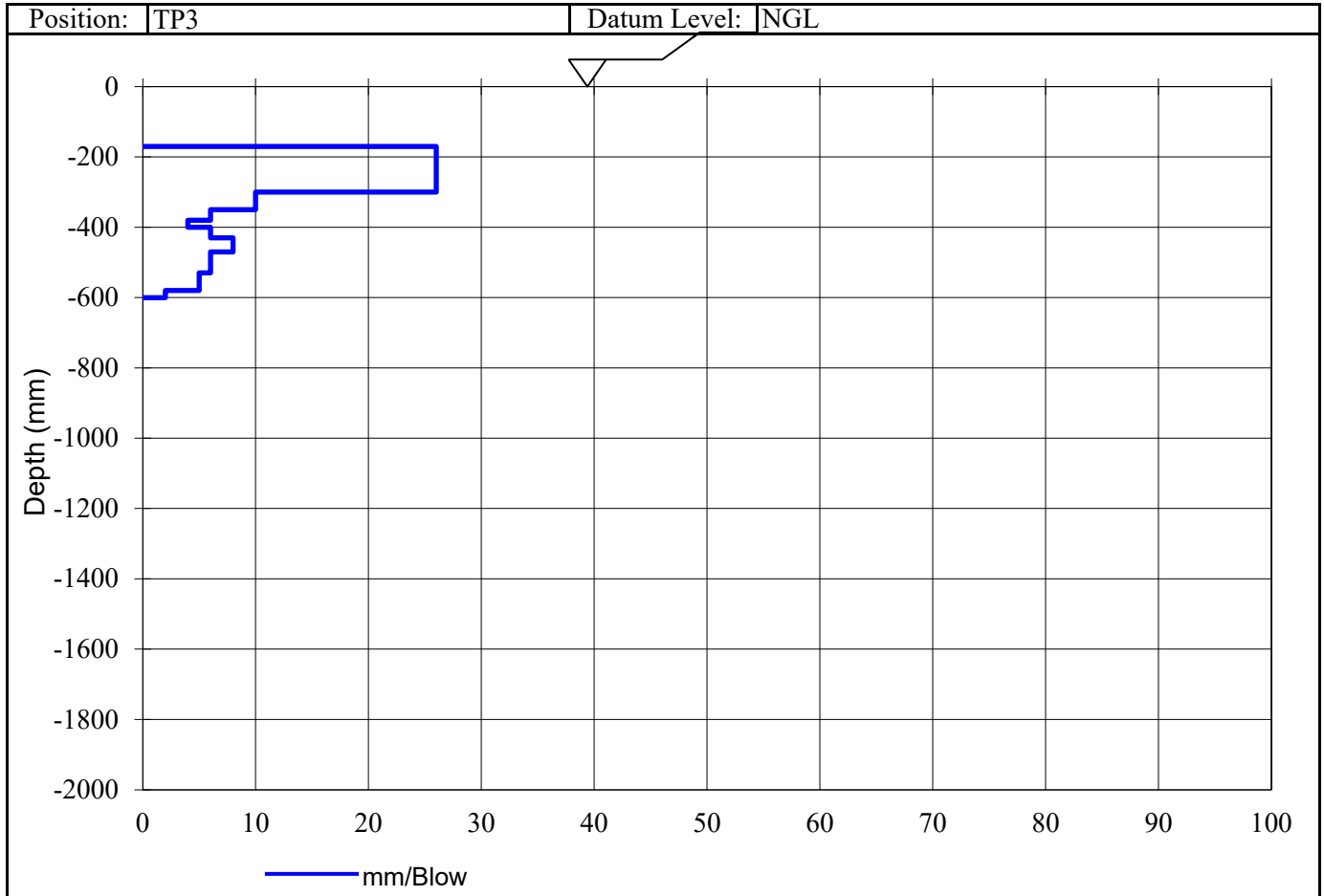
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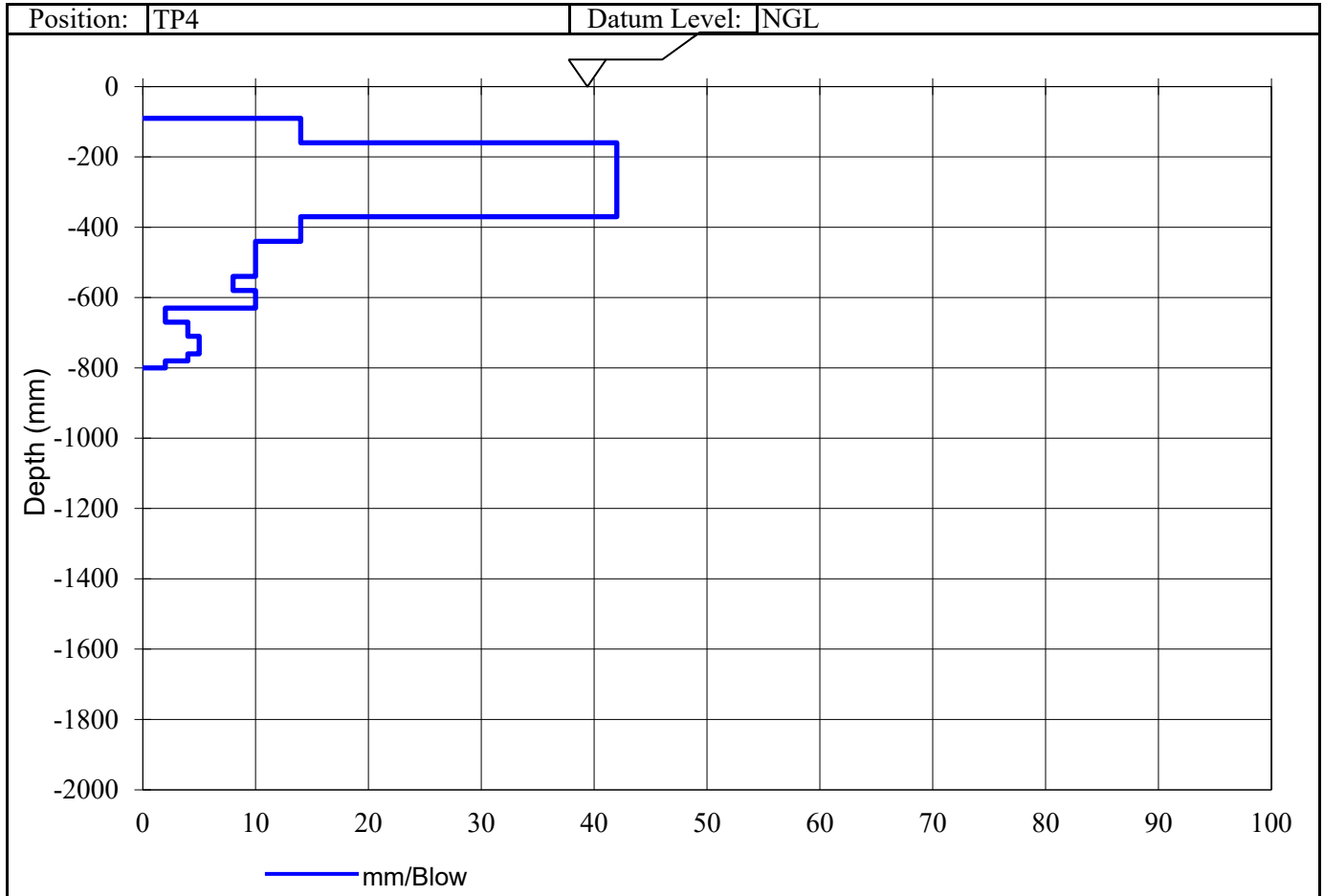
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Attention :	Wentzel Coetzee	No. of Pages :	4 of 6

TEST REPORT

Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



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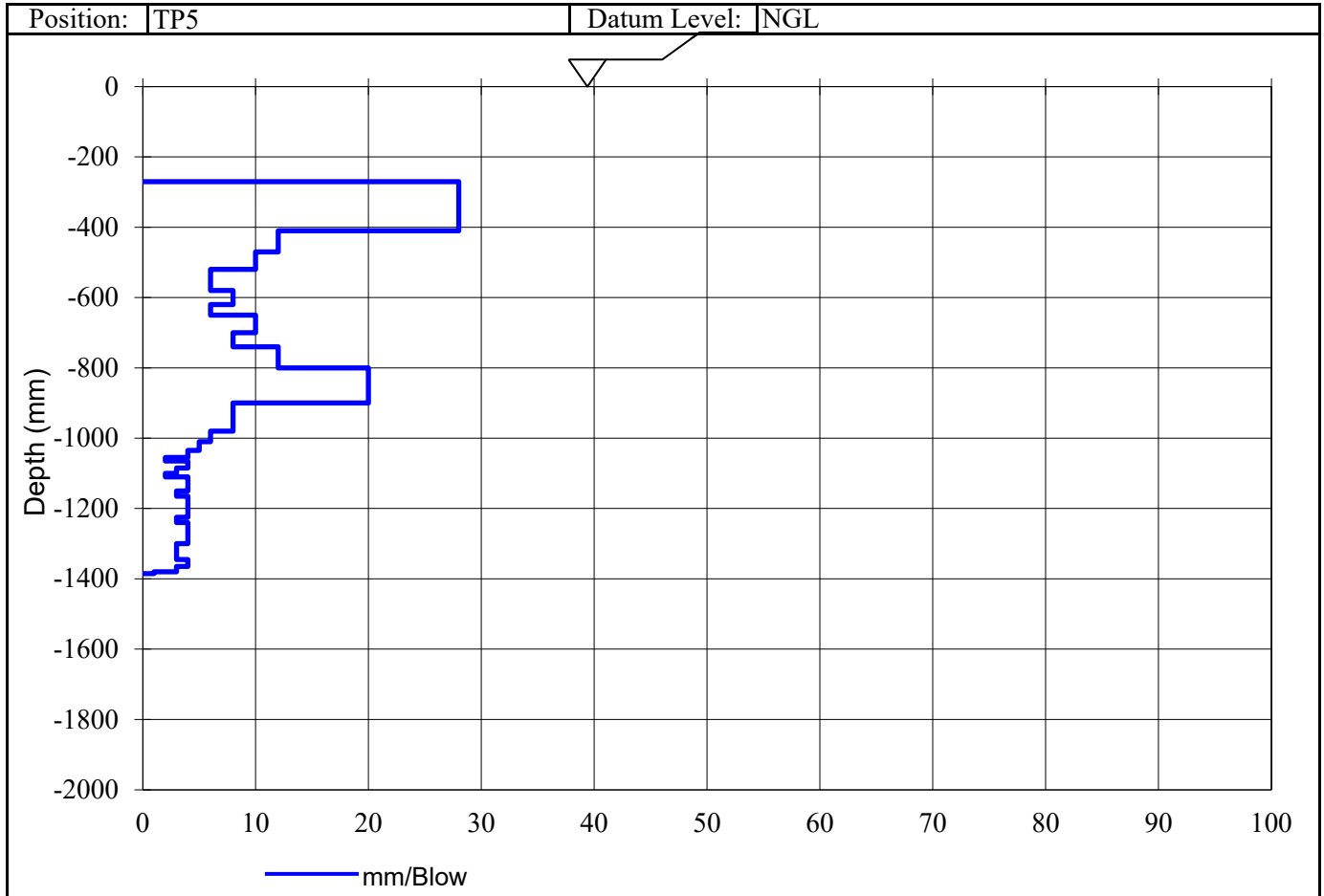
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	Wentzel Coetzee	No. of Pages :	5 of 6

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Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



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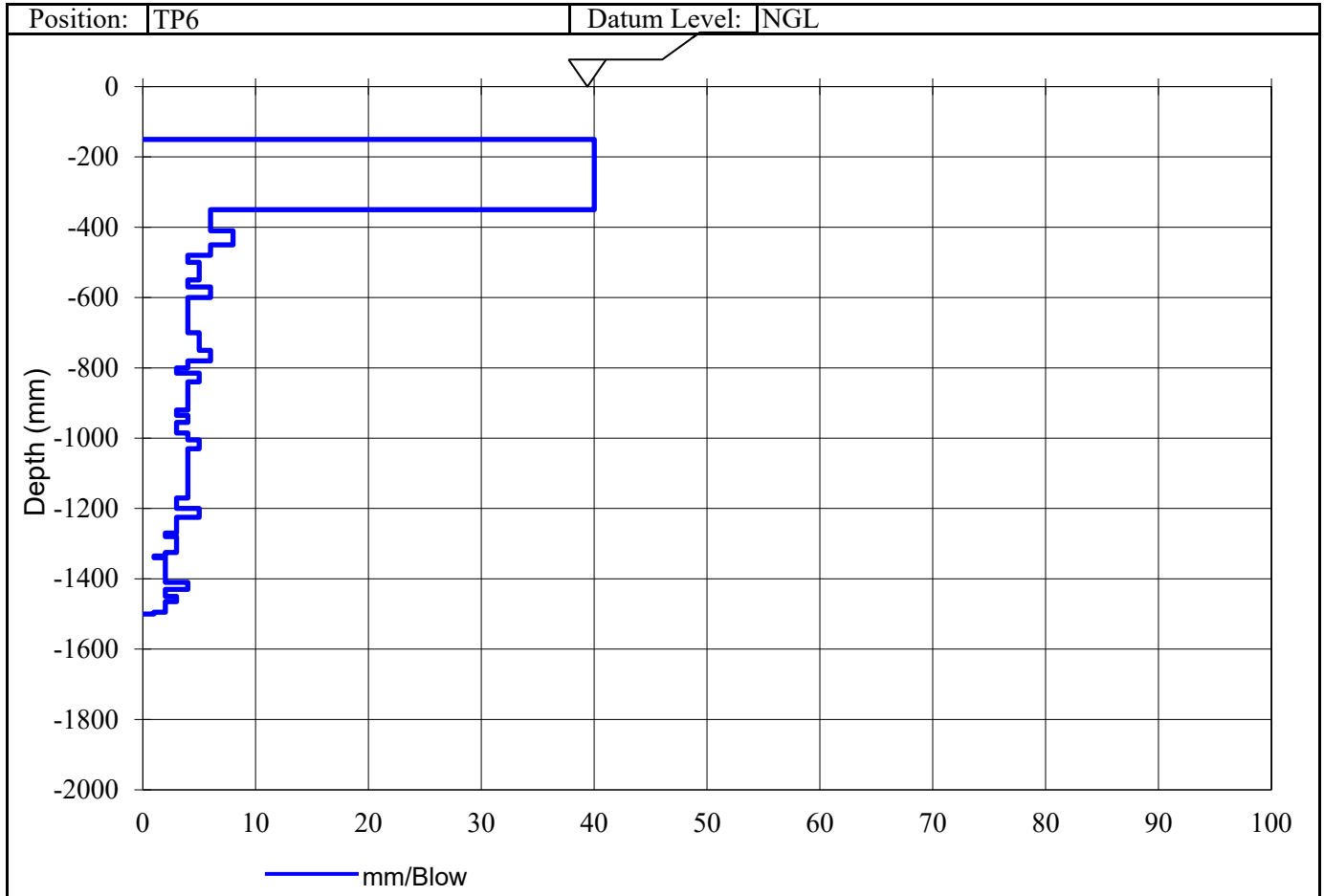
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	P.O. Box 401780	Date Received :	19.07.2021
	Gabrone	Date Reported :	23.07.2021
	Botswana	Req. Number :	
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TEST REPORT

Dynamic Cone Penetrometer (DCP) - (TMH 6 Method ST6)



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